Kelly & Associates

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TECHNICAL MEMORANDUM

To:Honeycreek Venetian, LLC
c/o Steve Lenart
Lenart Development Company, LLCFrom:Rod Kelly, P.E.
Kelly & AssociatesDate:October12, 2020RE:Traffic Impact Analysis – Proposed Weston Trails Residential Development in

Weston, Texas



A. Purpose

The purpose of this memorandum is to document the results of a traffic impact analysis (TIA) for the proposed Weston Trails residential development in Weston, Texas. This analysis was prepared to determine the possible impacts of the proposed development change on traffic operations at the access street intersections in the vicinity of this development. The analysis summarizes the findings, conclusions, and recommendations of the TIA and will be provided for technical review to fulfill the associated requirements of the local project approval process.

B. Methodology

The study methodology applied to the analysis was as follows:

- Conducted traffic counts to establish existing traffic volumes at the street intersections within the proposed Study Area
- > Estimated the vehicle trips in and out of proposed development
- Determined the analysis years based on the proposed phased completion of the residential construction and expected occupancy
- Determined the directions of approach and departure for traffic coming to and leaving the development
- Applied the proposed traffic growth rate to the non-site traffic for the agreed-upon analysis years and determined the non-site traffic volumes for the analysis years
- Combined the highest AM or PM peak hour non-site volumes and the volumes that will be generated by the development at the intersections to be analyzed for the analysis years
- > Determined the traffic lane configurations and intersection traffic control for the analysis years
- Entered the above traffic information as input data into Trafficware's "Synchro" traffic analysis software package, for conditions that included the traffic added by the proposed development
- > Determined adequacy of access roadway spacing and intersection sight distances
- > Tabulated the results and developed impact conclusions and any mitigation recommendations

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II. Existing and Proposed Land Use

A. Site Location / Study Area

The residential development is proposed to be located at the northeast quadrant of the intersection of FM 543 and CR 206 in Weston, Texas (See **Figure 1**). The proposed development site plan is shown in **Figure 2**. This TIA was only conducted for traffic generated by the proposed residential development property. The proposed construction program schedule is shown in **Table 1**





Figure 2 – Development Site Plan



| End of Year | # of Homes per year | Cum. # of Homes | Cum. # of PM Peak Hour Vehicle Trips |
|-------------|---------------------------|--------------------|--|
| 2021 | 213 | 213 | 211 |
| 2022 | 250 | 463 | 458 |
| 2023 | 250 | 713 | 706 |
| 2024 | 250 | 963 | 953 |
| 2025 | 272 | 1,235 | 1,223 |
| Total | 1235 | 1,235 | 1,223 |

Table 1 – Development Site Construction Schedule

The extent of the study area includes all six (6) of the proposed development access street intersections and the existing FM 543 and CR 206 intersection. These intersections are listed below and shown in **Figure 2**:

- CR 206 and FM 543
- CR 206 and Street 1
- CR 206 and Street 2
- CR 206 and Street 3
- FM 543 and Street 4
- FM 543 and Street 5
- FM 543 and Street 6

B. Existing Development

As shown in **Figure 1**, the site is currently undeveloped in a sparsely populated rural area. There are large lot, multi-acre, single family residences scattered throughout the area. The center of the small town of Weston is located approximately two miles north of the proposed development site.

III. EXISTING AND PROPOSED TRANSPORTATION SYSTEM

A. Thoroughfare System

FM 543 is currently a two-lane, north-south, undivided rural roadway from the Laud Howell Pkwy. connection to US 75 to the City of Weston. CR 206 is a two-lane, generally east-west, undivided rural roadway from FM 543 eastward and southward to connect with Weston Road. As shown in the Collin County Thoroughfare Plan, FM 543 and CR 206 are planned as six-lane, divided major arterials bordering on the west and south of the proposed development, respectively, of the proposed development. These two roadway facilities are highlighted by the red circle on the thoroughfare plan provided in **Appendix A**.

B. Existing Traffic Volumes

Vehicle traffic counts were obtained to establish existing traffic volumes in the vicinity of the six (6) development access street intersections with FM 543 and CR206. The vehicle counts were made on Thursday, August 13, at the intersection of FM 543 with CR 206 during the morning and afternoon peak traffic periods. The 2020 AM and PM peak hour traffic volume counts are provided in **Appendix B** and summarized in **Figure 3** at the end of this section.

C. Projected Traffic Volumes

Based on the home construction schedule and expected occupancy provided by the builder shown in **Table 1**, the traffic analysis years were determined. The first 213 homes are expected to be

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constructed and occupied by the end of 2021. Thereafter, 250 homes per year are expected to be built and occupied until the last of the homes are completed and occupied by the end of 2025. At the request of the developer, the analyses of traffic conditions were conducted in the latter part of Year 2021, after the first 213 homes in Phase 1 of the development scheduled to be built and occupied, and at the end of Year 2025, when all 1235 homes are scheduled to be completed and occupied.

To determine the projected background traffic volumes, TxDOT AADT traffic count data was obtained for a count station on FM 543, south of CR 125 (the closest count station to the project site) and calculated the annual changes in traffic volumes (increases and decreases) to come up with an average annual percentages change. As shown in the **Table 1** calculations below, the 5-year annual growth rate in non-site traffic was calculated to be 3.14%; therefore, a growth rate of 3% was used. The projected non-site 2021 and 2024 AM and PM peak hour traffic volumes are shown in **Figure 4** through **Figure 7** at the end of this section. The calculations for determining the projected background traffic volumes are provided in **Appendix B**.

| 5 Year G (AD | rowth Rate T) on FM 5 | of Average Dai 43 South of CR | ly Traffic 125 |
|-----------------|--------------------------|----------------------------------|-------------------|
| Year | ADT | Change | % Change |
| 2015 | 1340 | | |
| 2016 | 1433 | 93 | 6.94% |
| 2017 | 1800 | 367 | 25.61% |
| 2018 | 1800 | 0 | 0.00% |
| 2019 | 1440 | -360 | -20.00% |
| Avg. | | | 3.14% |
| Use | | | 3.00% |

Table 1 – Total Growth to Analysis Years

V.SITE TRAFFIC CHARACTERISTICS

A. Proposed Site Traffic Generation

According to the 9th Edition of the ITE Trip Generation Manual, the AM weekday peak hour trip generation rate is 0.74 trips per dwelling unit and the PM weekday peak hour trip generation rate is 0.99 trips per dwelling unit. Since the PM peak hour will generate the most traffic and the existing non-site traffic was found to be relatively light, it was decided to only analyze the heavier PM peak hour traffic conditions. The proposed 1235 homes in the residential development will ultimately generate a total of 1223 vehicle trips in the PM peak hour. With a PM peak hour directional distribution of 63 % inbound and 37% outbound vehicles, the PM peak hour inbound and outbound trips, when the site is fully developed, will be 770 and 452, respectively. The PM peak hour trips generated by the residential development, for each of the analysis years, are shown below in **Table 2**.

| Year | Land Use | ITE | Dwelling | PM Peak | Hour | PM | Peak Hour | PM Pea Pere | ak Hour cent | PM Peak Trips | Hour |
|------|----------|------|----------|---------|------|----|-----------|----------------|-----------------|------------------|------|
| | | Code | Units | т пр ка | ite | | tai irips | In | Out | In | Out |
| 2021 | SF Homes | 150 | 213 | 0.99 | | | 211 | 63% | 37% | 133 | 78 |
| 2025 | SF Homes | 150 | 1235 | 0.99 | | | 1223 | 63% | 37% | 770 | 453 |

Table 2 – Development Trip Generation

B. Trip Distribution and Traffic Assignment

The directions of approach and departure for the development traffic during the PM peak hour period, were derived from examining the other existing residential developments within a 4-mile radius and their accessibility to the regional roadway system and the distribution of traffic from the traffic counts referenced in **Section III.B Existing Traffic Volumes**, above. Based on this

information, the estimated general approach and departure traffic patterns were developed for the proposed residential development site and are shown in **Table 3**.

| Directions | In | Out |
|------------|--------|------|
| Directions | % From | % To |
| North | 5% | 5% |
| South | 60% | 60% |
| East | 30% | 30% |
| West | 5% | 5% |
| Total | 100% | 100% |

Table 3 – Directional Distribution of Development Traffic

Trips generated by the development were then assigned to the approaches of the intersections to be analyzed for the analysis years. The 2021 and 2025 AM and PM peak hour volumes are shown in **Figure 8** and **Figure 11**, at the end of this section

The projected AM and PM peak hour non-site traffic volumes and those that will be generated by the development at the intersections to be analyzed were combined for the two analysis years. These volumes are shown in **Figure 12** through **Figure 15** at the end of this section. The calculations for determining the combined projected Site + Non-Site traffic volumes are provided in **Appendix B**.

The traffic lane configurations and intersection traffic control were also determined and are displayed in **Figure 16** at the end of this section. The results were then tabulated, discussed, mitigation measures identified and applied if required, and capacity analyses re-run to verify acceptable operating levels of service, and conclusions developed to determine the impact of the added traffic.



Figure 3 – Existing 2020 AM & PM Peak Hour Traffic Volumes



Figure 4 – AM Peak Hour Non-Site Traffic for Year 2021







Figure 7 – PM Peak Hour Non-Site Traffic for Year 2025

















Figure 13 – PM Peak Hour Site + Non-Site Traffic for Year 2021





Figure 14 – AM Peak Hour Site + Non-Site Traffic for Year 2025



Figure 15 – PM Peak Hour Site + Non-Site Traffic for Year 2025



Figure 16 – Traffic Lane Configurations & Traffic Control for Year 2021 & 2025

V. TRAFFIC ANALYSIS AND MITIGATION

A. Level of Service Evaluations

The analysis of impacts is measured in terms of traffic operating level of service (LOS). According to the <u>Highway Capacity Manual (HCM)</u>, capacity is defined as the maximum number of vehicles that can be expected to travel on a given section of roadway or a specific lane during a given period under prevailing traffic conditions. The operational conditions of roadways are measured in terms of "Level of Service" (LOS). Level of Service refers to the operational conditions within a traffic stream and their perception by motorists in terms of delay, freedom to maneuver, traffic interruptions, comfort, convenience, and safety. There are six levels of service (LOS) or capacity conditions for each roadway facility and they are designated from "A" to "F", with "A" representing an optimal, free-flow condition, and "F" representing a congested, forced flow condition. These Delay/LOS relationships are shown in **Table 4** for intersections with stop sign and traffic signal control

| Average Vehicle Delay (Seconds) | LOS (Vol./Cap. Ratio) |
|---|--|
| per Vehicle for Stop Controlled Intersections | < or = to 1 |
| < or = to 10 | A |
| >10 & < or = 15 | В |
| >15 & < or = 25 | С |
| >25 & < or = 35 | D |
| >35 & <or 50<="" =="" td=""><td>E</td></or> | E |
| >50 | F |
| | |
| Average Vehicle Delay (Seconds) | LOS (Vol./Cap. Ratio) |
| Average Vehicle Delay (Seconds) Per Vehicle for Signalized Intersections | LOS (Vol./Cap. Ratio) <or 1<="" =="" td="" to=""></or> |
| Average Vehicle Delay (Seconds) Per Vehicle for Signalized Intersections < or = to 10 | LOS (Vol./Cap. Ratio) <or 1<br="" =="" to="">A</or> |
| Average Vehicle Delay (Seconds) Per Vehicle for Signalized Intersections < or = to 10 >10 & < or = 20 | LOS (Vol./Cap. Ratio) <or 1<br="" =="" to="">A B</or> |
| Average Vehicle Delay (Seconds) Per Vehicle for Signalized Intersections < or = to 10 >10 & < or = 20 >20 & < or = 35 | LOS (Vol./Cap. Ratio) <or 1<br="" =="" to="">A B C</or> |
| Average Vehicle Delay (Seconds) Per Vehicle for Signalized Intersections< or = to 10 | LOS (Vol./Cap. Ratio) <or 1<br="" =="" to="">A B C D</or> |
| Average Vehicle Delay (Seconds) Per Vehicle for Signalized Intersections< or = to 10 | LOS (Vol./Cap. Ratio) <or 1<br="" =="" to="">A B C C D E</or> |

Table 4 Relationship between Delay and LOS

The projected PM peak hour non-site traffic volumes in the latter part of 2021 were added to the volumes that will be generated by homes built and occupied in Phase 1 of the development in the same year, as shown in **Figure 8**, and the intersections analyzed, applying the expected lane configurations and traffic control shown in **Figure 10**. It should be noted that, where heavy turning volumes were expected to enter the development, separate right turn lanes were assumed to be added. The traffic information was then entered as input data into Trafficware's "Synchro" traffic analysis software package, for conditions that included the traffic added by the proposed development. A summary of the analysis results is shown in **Table 5**.

| • • • • | | AM / PM Pe | ak Hour No M | itigation) | AM / PM Pe | ak Hour (W / Mi | tigation) |
|---------|----------|---------------------|--------------|-----------------|------------|---------------------|-----------------|
| Inters | ection | Intersection LOS | Approach | Approach LOS | Mitigation | Intersection LOS | Approach LOS |
| | | | WB | B/B | Nana | | |
| CR 206 | FM543 | A / A | NB | A/A | Required | | |
| | | | SB | A/A | Required | | |
| | | | EB | A/A | Nama | | |
| CR 206 | Street 1 | A/A | WB | A/A | Required | | |
| | | | SB | A/A | Required | | |
| | | | EB | A/A | Nege | | |
| CR 206 | Street 2 | A / A | WB | A/A | Required | | |
| | | | SB | A/A | Required | | |
| | | | EB | A/A | Nono | | |
| CR 206 | Street 3 | A / A | WB | A/A | Required | | |
| | | | SB | A/A | required | | |

Table 5 – Year 2021 AM & PM Peak Hour Site + Non-Site Traffic Analysis Results

As can be seen from the results in **Table 5**, the traffic operations in latter part of 2021, for the intersections analyzed, are all estimated to operate at LOS B, or better. All intersection approaches are estimated to operate at LOS B or better. The detailed analysis work sheets are provided in **Appendix C1**.

Next, the PM peak hour non-site traffic volumes in 2025, at the time of full development, were added to the volumes that will be generated by the development, as shown in **Figure 9**, and the intersections analyzed with the lane configurations and traffic control shown in **Figure 11**. A summary of the analysis results is shown in **Table 6**.

| | AM & PM | Peak Hour (With | nout Mitigation | n) | AM & PM Pe | ak Hour (With N | litigation) |
|---------|----------------|---------------------|-----------------|------------------|---------------|---------------------|-----------------|
| Interse | ection | Intersection LOS | Approach | Approach LOS/ | Mitigation | Intersection LOS | Approach LOS |
| | | | WB | D/E | Northbound | | C/C |
| CR 206 | FM 543 | A/A | NB | A/A | Right Turn | A/A | A/A |
| | | | SB | A / A | Lane Added | | A/A |
| | Street | | EB | A / A | | | |
| CR 206 | Street | A/A | WB | A/A | None Required | | |
| | • | | SB | A / A | | | |
| | Chroat | | EB | A / A | | | |
| CR 206 | Street | A/A | WB | A/A | None Required | | |
| | 2 | | SB | A/A | | | |
| | 0 , , | | WB | A/A | | | |
| CR 206 | Street | A/A | NB | A/A | None Required | | |
| | 5 | | SB | B/B | | | |
| | 01 | | WB | B/B | | | |
| CR 206 | Street | A/A | NB | A/A | None Required | | |
| | - | | SB | A/A | | | |
| | 0 | | WB | B/B | | | |
| CR 206 | Street | A/A | NB | A/A | None Required | | |
| | 5 | | SB | A/A | | | |
| | 0 , , , | | WB | B/B | | | |
| CR 206 | Street | A/A | NB | A/A | None Required | | |
| | 0 | | SB | A/A | | | |

 Table 6 – Year 2025 AM & PM Peak Hour Site + Non-Site Traffic Analysis Results

As can be seen from the unmitigated results in **Table 6**, the traffic operations in 2025, for the intersections and intersection approaches analyzed, are all estimated to operate at LOS C, or better, except for an LOS D and E for the westbound approach of CR 206 at the FM 543 intersection in the AM and PM peak traffic hours, respectively. The detailed analysis work sheets are provided in **Appendix C2**.

Given the undesirable level of service on the westbound approach of CR 206 at FM 543 intersections, mitigation measures known to address this condition was tested. The mitigation was to add a separate right turn lane on the northbound approach of FM 543. Since NB is free flow, separating the heavy RTs out eliminates the conflict between them and the WB approach. Now WB only must find gaps in the NB thru traffic. The proposed mitigation measure is shown in orange in **Figure 12** and the results of the analyses are shown in the AM and PM Peak Hours (With Mitigation) section of **Table 6**. The detailed analysis work sheets are shown in **Appendix C3**.



Figure 12 – NB FM 543 Right Turn Lane Mitigation

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B. Analysis of Development Access Street Intersection Turn Lane Requirements Given the uncertainty of the schedule of roadway improvements+ associated with the City of Weston and Collin County Thoroughfare Plans, as discussed in **Section III.A**, the need for turn lanes on FM 543 and CR 206 to serve the development access was examined for the proposed access schemes. The analysis of development access turn lanes using the Texas Department of Transportation (TxDOT) Access Management Manual and Roadway Design Manual, which contains criteria for right and left turn lanes on highways, was applied to the proposed development site. Chapter 2, <u>Access Management Standards</u>, in the Access Management Manual and Chapter 3, New <u>Location and Reconstruction (4R) Design Criteria</u>, in the Roadway Design Manual, present thresholds for these auxiliary lanes. The relevant sections of these documents referenced in the following discussions are provided in **Appendix D**.

<u>Right Turn Lane Requirements</u> - For right turn lanes, Table 2-3, on page 2-14 of the TxDOT Access Management Manual indicates that the threshold for right-turn deceleration lanes on roadways with posted speed limits above 45 mph is <u>50 vehicles per</u> hour (vph). **Table 7** shows the right-turn volumes at the street or driveway that exceed the hourly threshold for the 2021 and 2025 analysis year.

| Intersection | Арр | roach | Posted Speed | Hourly Threshold | AM Vol | RT ume | PM Volu | RT ume |
|----------------------|------|-------|-----------------|---------------------|-----------|-----------|------------|-----------|
| | 2021 | 2025 | | | 2021 | 2025 | 2021 | 2025 |
| FM 543 @ CR 206 | NB | NB | 55 mph | 50 vph | | 105 | 121* | 344 |
| FM 543 @ Street 4 | | NB | 55 mph | 50 vph | 1 | 1 | ł | 91 |
| FM543 @ Street 5 | | NB | 55 mph | 50 vph | - | - | - | 61 |
| FM 543 @ Street 6 | | NB | 55 mph | 50 vph | | | | 91 |

Table 7 – Year 2021 & 2025 AM & PM Peak Hour Right Turn Lane Needs

Applying TxDOT criteria, the information in this **Table 7** indicates that a northbound right turn lane will be warranted in the PM peak hour in 2021, with the completion of Phase 1; however, the HCM intersection capacity analysis results shows that LOS A traffic conditions will exist at that intersection. In addition, the TxDOT criteria is shown to warrant right turn lanes on the northbound approach of FM543 at CR 206 in both the 2025 AM and PM peak hour, while HCM capacity analysis indicates that the northbound approach of FM 543 at Streets 4, 5, and 6 in the PM peak hour, while HCM capacity analysis indicates that the northbound approach of FM 543 at CR 206.

<u>Left Turn Lane Requirements</u> – Applying TxDOT criteria and based on PM peak hour Site + Non-Site traffic volumes for buildout year 2025, shown in **Figure 15**; the need for separate left turn lanes, were evaluated for traffic southbound on FM 543 and eastbound on CR 206 to enter the proposed development. Based on the HCM intersection analysis results and the low left turn volumes, year 2021 left turn needs for eastbound CR 206 were not analyzed. The results of these evaluations are shown in **Table 8**.

| Intersection | Advancing Volume | Percent Left Turns | Opposing Volume | Table Value | Table Value More or Less | Left Turn Lane Warranted |
|----------------------|---------------------|-----------------------|--------------------|----------------|-----------------------------|--------------------------------|
| CR 206 @ Street 1 | 137 | 88 | 31 | 240+ | More | No |
| CR 206 @ Street 2 | 254 | 48 | 96 | 240+ | Less | Yes |
| CR 206 @ Street 3 | 371 | 33 | 161 | 215+ | Less | Yes |
| FM 543 @ Street 4 | 165 | 3 | 272 | 450+ | More | No |
| FM 543 @ Street 5 | 133 | 2 | 214 | 450+ | More | No |
| FM 543 @ Street 6 | 85 | 6 | 125 | 505 | More | No |

Table 8 – Year 2025 PM Peak Hour Left Turn Lane Needs Analysis

Applying the traffic information in these figures to Table 3-11, on page 3-37 of the TxDOT Roadway Design Manual provided in **Appendix D** to the volumes shown in **Figure 15**, it can be seen that only two of the estimated Year 2025 advancing volumes are higher than the left turn table values, while HCM capacity analysis LOS results in **Table 6**, don't show any need for left turn lanes in the 2025 PM peak hour.

VI. CONCLUSIONS AND RECOMMENDATIONS

A. Conclusions

Based upon the Analysis Findings described above, the following conclusions can be drawn.

<u>Intersection Levels of Service</u> – The overall intersection Levels of Service (LOSs) at the seven intersections analyzed for the AM and PM peak hours with Year 2021 and Year 2025 traffic conditions, development traffic added, and no mitigation; were found to be all at LOS A.

<u>Approach Levels of Service</u> - On an approach basis, the only approach that had an LOS below C was the westbound approach of the intersection of FM 543 and CR 206, with an LOS D in the AM peak hour and an LOS E in the PM peak hour and Year 2025 traffic conditions. This condition is expected to be alleviated by the addition of a northbound right turn lane at that intersection. Since the northbound traffic is free flow, separating the heavy right turns out eliminates the conflict between them and the westbound approach so that the westbound approach traffic only must find gaps in the northbound thru traffic.

<u>Right Turn Lane Requirements</u> - Based on the TxDOT criteria, northbound right turn lanes are expected to be warranted by development buildout Year 2025 at the FM 543 intersections with CR 206 and development access Streets 4, 5, and 6 by Year 2025. However, as explained in the above <u>Approach Level of Service</u> section of the Conclusions, the HCM capacity analysis LOS results only show a need for a northbound right turn lane at the intersection of FM 543 and CR 206 in the 2025 AM & PM peak hour.

<u>Left Turn Lane Requirements</u> - Based on TxDOT roadway design manual criteria, no left turn lanes are expected to be needed for Phase 1 of the development in 2021. Left turn lanes are shown to be warranted on eastbound CR 206 at development access Streets 2 and 3 at the development buildout Year 2025. However, HCM capacity analysis LOS results don't show any need for separate left turn lanes in 2025.

<u>Driveway Location and Spacing</u> - The driveway spacings meet TxDOT access management spacing criteria of 425 feet on FM 543 and CR 206 for the posted speed limits.

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<u>Sight Distances</u> - The generally flat terrain and straight roadway alignments in both directions from the proposed development driveways will provide the required intersection sight distances.

B. Recommendations

During the initial stages of development construction, existing traffic lanes and stop sign control at the development access streets intersections with FM 543 are expected to be adequate. However, an additional northbound right turn traffic lane at the intersections FM 543 and CR 206 appears to be needed when the development is built out and occupied. Never the less, given these findings and the uncertainty of the schedule of roadway improvements associated with the City of Weston and Collin County Thoroughfare Plans, the need for mitigation measures should be verified with up-to-date signal warrant studies and intersection capacity analyses, with traffic counts, as the buildout year approaches or if traffic conditions deteriorate to the point that mitigation measures appear to be needed earlier than expected.

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Appendices

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Appendix A

Thoroughfare Plan Map



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Appendix B

Existing Traffic Volume Counts and 2021 & 2025 AM & PM Peak Period Traffic Volumes

| | 07.001 | | | T oranie | | |
|---------------------|--------|-------|-------|-----------------|-------|-------|
| Leg | FM | 543 | CR | 206 | FM | 543 |
| Direction | South | bound | West | bound | North | bound |
| Start Time | Thru | Left | Right | Left | Right | Thru |
| 2020-08-13 07:30:00 | 11 | 0 | 0 | 1 | 0 | 13 |
| 2020-08-13 07:45:00 | 16 | 0 | 1 | 0 | 0 | 16 |
| 2020-08-13 08:00:00 | 12 | 0 | 0 | 1 | 0 | 5 |
| 2020-08-13 08:15:00 | 10 | 0 | 0 | 1 | 3 | 11 |
| Grand Total | 49 | 0 | 1 | 3 | 3 | 45 |

2020 AM Peak Hour Traffic Volumes

2020 PM Peak Hour Traffic Volumes

| Leg | FM | 543 | CR | 206 | FM | 543 |
|---------------------|-------|-------|-------|-------|-------|-------|
| Direction | South | bound | West | bound | North | bound |
| Start Time | Thru | Left | Right | Left | Right | Thru |
| 2020-08-13 17:15:00 | 14 | 1 | 0 | 1 | 0 | 11 |
| 2020-08-13 17:30:00 | 15 | 0 | 1 | 0 | 1 | 12 |
| 2020-08-13 17:45:00 | 18 | 0 | 1 | 0 | 1 | 16 |
| 2020-08-13 18:00:00 | 12 | 0 | 0 | 1 | 1 | 16 |
| Grand Total | 59 | 1 | 2 | 2 | 3 | 55 |

| | AMF | Peak Hour Volui | mes - CR 20 | 06 / Westor | 1 Trails Resi | idential St | reet 1 | | Γ | | A | M Peak Hour | Volumes - (| R 206 / Wes | ton Trails Re | sidential | Street 2 | | |
|---------|--------------------|----------------------|-------------|-------------|---------------|-------------|--------|--------|---------|----------|--------------------|--------------------|-------------|-------------|---------------|-----------|----------|-------|----------|
| ovement | 2021 Multiplier | 2025 Multiplier | | Non-site | | S. | te | N+ S-N | TR Site | Movement | 2021 Multiplier | 2025 Multiplier | | Non-site | | S | ite | N+S-N | NTR Site |
| | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 | | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 |
| EBL | 1.03 | 1.16 | 0 | 0 | 0 | 12 | 36 | 12 | 36 | EBL | 1.03 | 1.16 | 0 | 0 | 0 | 13 | 36 | 13 | 36 |
| EBT | 1.03 | 1.16 | ŝ | ŝ | e | 4 | 24 | 7 | 27 | EBT | 1.03 | 1.16 | ß | s | 3 | 14 | 54 | 17 | 57 |
| WBT | 1.03 | 1.16 | 1 | 1 | 1 | 2 | 4 | 3 | 2 | WBT | 1.03 | 1.16 | 1 | 1 | 1 | 38 | 109 | 39 | 110 |
| WBR | 1.03 | 1.16 | 0 | 0 | 0 | 1 | 2 | 1 | 2 | WBR | 1.03 | 1.16 | 0 | 0 | 0 | 1 | 2 | 1 | 2 |
| SBL | 1.03 | 1.16 | 0 | 0 | 0 | 2 | 9 | 2 | 9 | SBL | 1.03 | 1.16 | 0 | 0 | 0 | 2 | 9 | 2 | 9 |
| SBR | 1.03 | 1.16 | 0 | 0 | 0 | 37 | 107 | 37 | 107 | SBR | 1.03 | 1.16 | 0 | 0 | 0 | 38 | 107 | 38 | 107 |
| | | | | | | | | | | | | | | | | | | | |
| | AME | Peak Hour Volu | mes - CR 20 | 06 / Westol | n Trails Res | idential St | reet 3 | | Γ | | | A | M Peak Hou | r Volumes - | CR 206 / FM | 543 | | 100 | |
| vement | 2021 Multiplier | 2025 Multiplier | | Non-site | | S | te | N+ S-N | TR Site | Movement | 2021 Multiplier | 2025 Multiplier | | Non-site | | s | ite | 1+S-N | NTR Site |
| | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 | | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 |
| EBL | 1.03 | 1.16 | 0 | 0 | 0 | 13 | 36 | 13 | 36 | WBL | 1.03 | 1.16 | 1 | 1 | 1 | 106 | 305 | 107 | 306 |
| EBT | 1.03 | 1.16 | e | 3 | 3 | 25 | 84 | 28 | 87 | WBR | 1.03 | 1.16 | 1 | 1 | 1 | 9 | 20 | 7 | 21 |
| WBT | 1.03 | 1.16 | 1 | 1 | 7 | 75 | 214 | 76 | 215 | NBT | 1.03 | 1.16 | 33 | 34 | 38 | 0 | 99 | 34 | 104 |
| WBR | 1.03 | 1.16 | • | 0 | • | 1 | 2 | 1 | 2 | NBR | 1.03 | 1.16 | 2 | 2 | 2 | 35 | 103 | 37 | 105 |
| SBL | 1.03 | 1.16 | 0 | 0 | 0 | 2 | 9 | 2 | 9 | SBL | 1.03 | 1.16 | 1 | 1 | 1 | 5 | 17 | 4 | 18 |
| SBR | 1.03 | 1.16 | 0 | • | 0 | 37 | 107 | 37 | 107 | SBT | 1.03 | 1.16 | 82 | 84 | 95 | 0 | 204 | 84 | 299 |
| | | AM Pea | ak Hour Vol | lumes - FM | 543 / Stree | it 4 | | | Γ | | | AM Pea | k Hour Volu | mes - FM 54 | 3 / Residenti | al Street | | | |
| ement | 2021 Multiplier | 2025 . Multiplier | | Non-site | | ŝ | te | N+ S-N | TR Site | Movement | 2021 Multiplier | 2025 Multiplier | | Non-site | | s | ite | N-S+1 | NTR Site |
| | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 | | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 |
| WBL | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 81 | 0 | 81 | WBL | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 53 | 0 | 53 |
| WBR | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | WBR | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 4 | 0 | 4 |
| NBT | 1.03 | 1.16 | 33 | 34 | 38 | 0 | 60 | 34 | 98 | NBT | 1.03 | 1.16 | 33 | 34 | 38 | 0 | 46 | 34 | 84 |
| NBR | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 26 | 0 | 26 | NBR | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 18 | 0 | 18 |
| SBL | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | SBL | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| SBT | 1.03 | 1.16 | 83 | 85 | 96 | • | 140 | 85 | 236 | SBT | 1.03 | 1.16 | 83 | 85 | 96 | 0 | 88 | 85 | 185 |
| | | AM Pea | ik Hour Vol | lumes - FM | 543 / Stree | st 6 | | | Γ | | | | | | | | | | |
| vement | 2021 Multiplier | 2025 Multiplier | | Non-site | | Si | te | N+ S-N | TR Site | | | | | | | | | | |
| | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 | | | | | | | | | | |
| WBL | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 81 | 0 | 81 | | | | | | | | | | |
| WBR | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | | | | | | | | | | |
| NBT | 1.03 | 1.16 | 33 | 34 | 38 | 0 | 24 | 34 | 62 | | | | | | | | | | |
| NBR | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 26 | 0 | 26 | | | | | | | | | | |
| SBL | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | | | | | | | | | | |
| SBT | 1.03 | 1.16 | 83 | 85 | 96 | 0 | 6 | 85 | 105 | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |

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| | PM Pea | hk Hour Volum | es - CR 20 | 5 / Weston | Trails Resid | lential S | reet 1 | | Γ | L | | PM Peak H | our Volumes | - CR 206 | / Weston | Trails Res | idential | Street 2 | | |
|---------|--------------------|--------------------|-------------|-------------|---------------------|-----------|---------|--------|----------|-------|----------|--------------------|--------------------|----------|------------|------------|----------|----------|-----------|--------|
| ovement | 2021 Multiplier | 2025 Multiplier | | Non-site | | | ite | N-S+1 | ATR Site | Moven | nent | 2021 Iultiplier | 2025 Multiplier | | Non-site | | Site | | LW + S-N | R Site |
| | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 | | | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 |
| EBL | 1.03 | 1.16 | 0 | 0 | 0 | 42 | 121 | 42 | 121 | E | BL BL | 1.03 | 1.16 | 0 | 0 | 0 | 43 | 121 | 43 | 121 |
| EBT | 1.03 | 1.16 | 2 | 2 | 2 | m | 14 | s | 16 | E | BT | 1.03 | 1.16 | 2 | 2 | 2 | 43 | 131 | 45 | 133 |
| WBT | 1.03 | 1.16 | 4 | 4 | ŝ | 4 | 26 | ∞ | 31 | M | BT | 1.03 | 1.16 | 4 | 4 | S | 26 | 91 | 30 | 96 |
| WBR | 1.03 | 1.16 | 0 | 0 | 0 | 2 | 9 | 2 | 9 | W | BR | 1.03 | 1.16 | 0 | 0 | 0 | 2 | 9 | 2 | 9 |
| SBL | 1.03 | 1.16 | 0 | 0 | • | - | 4 | 1 | 4 | SI | BL | 1.03 | 1.16 | 0 | 0 | 0 | 2 | 4 | 2 | 4 |
| SBR | 1.03 | 1.16 | 0 | • | • | 24 | 71 | 24 | 71 | S | BR | 1.03 | 1.16 | 0 | 0 | 0 | 26 | 71 | 26 | 71 |
| | | | | | | | | | | | | | | | | | | - | | |
| | | | | | | | | | ſ | | | | | | | | | 200 | | |
| | PM Pe | ak Hour Volun | tes - CR 20 | 6 / Weston | Trails Resi | dential 5 | treet 3 | | | | | | PM Peak H | our Volu | mes - CR 2 | 06 / FM | 543 | 1 | | |
| vement | 2021 Multiplier | 2025 Multiplier | | Non-site | | | ite | N+S+N | ATR Site | Moven | nent N. | 2021 Iultiplier | 2025 Multiplier | | Non-site | | Sit | 3 0 | LVN + S-N | R Site |
| | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 | | | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 |
| EBL | 1.03 | 1.16 | 0 | • | • | 42 | 121 | 42 | 121 | M | BL BL | 1.03 | 1.16 | 2 | 2 | 2 | 70 | 203 | 72 | 205 |
| EBT | 1.03 | 1.16 | 2 | 2 | ~ ~ | 85 | 248 | 87 | 250 | N I | BR | 1.03 | 1.16 | 2 | 2 | 2 | 4 | 24 | 9 10 | 26 |
| Idw | 50 T | OT'T | * 0 | * | | n · | OCT V | 50 | TOT | z | 19 | 1.03 | 0T.T | 35 | 56 | 101 | 0 | 230 | 5 | 33/ |
| SBI | 1.03 | 1 16 01.1 | | | | 7 | 0 4 | 7 | 0 | Z | BK | 1.03 | 1.16 | - | | - | 120 | 343 | 121 | 344 |
| SBR | 1.03 | 1.16 | 0 | 0 | • | 24 | 71 | 24 | 12 | 15 | 3T | 1 03 | 1 16 | 45 | 46 | 63 | 0 | 134 | 46 | 186 |
| | | | | | | | | | | | | | | | | | | | | |
| | | PM Peak | Hour Volu | imes - FM 5 | 43 / Street | 4 | | | | L | | PM | Peak Hour Vo | - samula | FM 543 / R | esidentia | I Street | 5 | | |
| vement | 2021 Multiplier | 2025 Multiplier | | Non-site | | | ite | \+ S-N | NTR Site | Moven | nent | 2021 ultiplier | 2025 Multiplier | | Non-site | | Stt | 8 | LW + S-N | R Site |
| | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 | | | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 |
| WBL | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 53 | 0 | 53 | M | BL | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 35 | 0 | 35 |
| WBR | 1.03 | 1.16 | 0 | • | 0 | 0 | ŝ | 0 | 8 | M | BR | 1.03 | 1.16 | 0 | 0 | 0 | 0 | 2 | 0 | 2 |
| NBT | 1.03 | 1.16 | 94 | 97 | 109 | 0 | 163 | 6 | 272 | Z | BT | 1.03 | 1.16 | 94 | 97 | 109 | 0 | 105 | 97 | 214 |
| NBK | 1.03 | 1.16 | 0 | | | 0 | 16 | • | 91 | Z | BR | 1.03 | 1.16 | 0 | 0 | • | 0 | 61 | 0 | 61 |
| SBT | 1.03 | 1.16 | 46 | 47 | 23 | 0 | 107 | 47 | 160 | SE | 8L 3T | 1.03 | 1.16 | 46 | 47 | 53 | 0 | 5 77 | 47 | 130 |
| | | | | | | | | | | | | | | | | | | | | |
| | | PM Peak | Hour Volu | ames - FM 5 | 43 / Street | 9 | | | | | | | | | | | | | | |
| vement | 2021 Multiplier | 2025 Multiplier | | Non-site | | | lite | N+S+N | ATR Site | | | | | | | | | | | |
| | | | 2020 | 2021 | 2025 | 2021 | 2025 | 2021 | 2025 | | | | | | | | | | | |
| WBL | 1.03 | 1.16 | 0 | • | 0 | • | 53 | 0 | 53 | | | | | | | | | | | |
| WBR | 1.03 | 1.16 | 0 | • | • | • | m | • | e | | | | | | | | | | | |
| NBT | 1.03 | 1.16 | 94 | 61 | 109 | • | 16 | 6 | 125 | | | | | | | | | | | |
| NBR | 1.03 | 1.16 | 0 | • | • | 0 | 91 | • | 91 | | | | | | | | | | | |
| SBL | 1.03 | 91.1 | | | | - | ~ | - | 2 | | | | | | | | | | | |
| 100 | SULL TUDS | OT'T | 40 | 141 | 22 | 2 | 17 | 14 | 80 1 | | | | | | | | | | | |

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Appendix C

Capacity Analysis Worksheets

Appendix C1

2021 AM & PM Traffic Conditions with Phase 1 Development

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| 1. FIVI 343 & CF | 1200 | , | | | | | AM 2021 Site + Non-Site |
|--|------------------|-----------------|----------------|--------|--------------------|---|-------------------------|
| | | | | | | 101 D. C. | |
| ntersection | 43 | 112512 | Sec. 2 | | | | |
| In Delay, aven | 11/01 | 14100 | A UP T | 100 | 201 | | |
| Movement | WBL | WBR | NBI | NBK | SBL | SBT | |
| Lane Configurations | 107 | 7 | 34 | 37 | 1 | 6 | |
| Future Vol. veh/h | 107 | 7 | 34 | 37 | 4 | 84 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | 0 | - | - | - | - | - | |
| Veh in Median Storage | 3,# 0 | - | 0 | - | - | 0 | |
| Jrade, % | 02 | 02 | 02 | - 02 | 02 | 02 | |
| Heavy Vehicles % | 32 | 32 | 92 | 32 | 32 | 92 | |
| Nymt Flow | 116 | 8 | 37 | 40 | 4 | 91 | |
| in the second se | | and the second | and the second | | Contraction of the | | |
| Major/Minor | Minor1 | a la catalana (| Agior1 | 1 | Major2 | | |
| Conflicting Flow All | 156 | 57 | 0 | 0 | 77 | 0 | |
| Stage 1 | 57 | - | - | - | | - | |
| Stage 2 | 99 | - | - | - | - | - | |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - | |
| Critical Hdwy Stg 1 | 5.42 | - | - | | - | - | |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - | |
| ollow-up Hawy | 3.518 | 3.318 | - | - | 2.218 | - | |
| Stage 1 | 966 | 1009 | - | - | 1522 | 10000 | |
| Stage 2 | 925 | - | - | - | | - | |
| Platoon blocked, % | No. and Constant | | - | - | | - | |
| Nov Cap-1 Maneuver | 832 | 1009 | - | - | 1522 | - | |
| Nov Cap-2 Maneuver | 832 | - | - | - | - | - | |
| Stage 1 | 963 | - | - | - | - | - | |
| Stage 2 | 920 | - | - | - | - | • | |
| and the second se | 14/17 | | AUD. | | | | |
| CM Control Dolov | 10 | | INB | | SB | | |
| ICM LOS | B | | U | | 0.5 | | |
| | | | | | | | |
| Ainor Lane/Major Mym | 1t | NRT | NRRV | WBI n1 | SRI | SBT | |
| anacity (veh/h) | 1 | - | - | 841 | 1522 | - | |
| ICM Lane V/C Ratio | | - | - | 0.147 | 0.003 | - | |
| ICM Control Delay (s) | | - | - | 10 | 7.4 | 0 | |
| ICM Lane LOS | | - | - | В | А | А | |
| ICM 95th %tile Q(veh) | | - | - | 0.5 | 0 | - | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |

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| ntersection nt Delay, s/veh | | | | | | | |
|--|--------|---------------------------------------|-------------------------|--------------------|--------------|--|--|
| nt Delay, s/veh | | | | | | | |
| in Dolaj, erren | 6.8 | | | | | | |
| | FDI | FOT | MOT | MIDD | 0.01 | 000 | |
| Movement | EBL | FRI | WBI | WBR | SBL | SBR | |
| ane Configurations | 40 | 4 | ef | 4 | TT. | 07 | |
| France Vol, ven/n | 12 | 7 | 3 | 1 | 2 | 3/ | |
| Conflicting Pede #/hr | 12 | 0 | 0 | 0 | 2 | 0 | |
| Sign Control | Free | Free | Free | Eree | Stop | Ston | |
| RT Channelized | - | None | - | None | otop - | None | |
| Storage Length | - | - | - | - | 0 | - | |
| /eh in Median Storage. | # - | 0 | 0 | | 0 | | |
| Grade, % | - | 0 | 0 | - | 0 | - | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| leavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| vivmt Flow | 13 | 8 | 3 | 1 | 2 | 40 | |
| | | | | | | | |
| Aaior/Minor | laior1 | A | laior? | N | linor? | | |
| Conflicting Flow All | Λ | 0 | ajuiz | 0 | 38 | 1 | |
| Stage 1 | 4 | 0 | - | 0 | 4 | 4 | |
| Stage 2 | | - | | | 34 | - | |
| Critical Hdwy | 4 12 | | | | 642 | 6.22 | |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - | |
| Critical Hdwy Stg 2 | | | | - | 5.42 | | |
| ollow-up Hdwy | 2.218 | - | - | • | 3.518 | 3.318 | |
| Pot Cap-1 Maneuver | 1618 | 000120 | - | - | 974 | 1080 | |
| Stage 1 | - | - | - | - | 1019 | - | |
| Stage 2 | • | - | - | - | 988 | - | |
| Platoon blocked, % | | - | - | - | | | |
| Nov Cap-1 Maneuver | 1618 | - | - | - | 966 | 1080 | |
| Nov Cap-2 Maneuver | - | × | - | - | 966 | | |
| Stage 1 | - | - | - | - | 1011 | - | |
| Stage 2 | - | - | | - | 988 | - | |
| CONTRACTOR OF A DESCRIPTION OF A DESCRIP | | | | | | | |
| | EP | | WB | | SB | | |
| Approach | ED | A LOUP AL CARDON | 0 | | 8.5 | | |
| Approach ICM Control Delay, s | 4.6 | | U | | CONTROL CAPE | | |
| Approach ICM Control Delay, s ICM LOS | 4.6 | | U | | A | | |
| Approach ICM Control Delay, s ICM LOS | 4.6 | | U | | Α | | |
| Approach ICM Control Delay, s ICM LOS | 4.6 | FBL | FRT | WRT | A | SBI n1 | |
| Approach ICM Control Delay, s ICM LOS Minor Lane/Major Mvmt | 4.6 | EBL | EBT | WBT | A WBR S | SBLn1 | |
| Approach ICM Control Delay, s ICM LOS Minor Lane/Major Mvmt Capacity (veh/h) ICM Lane V/C Ratio | 4.6 | EBL 1618 0.008 | EBT | WBT | A WBR | SBLn1 1074 | |
| Approach ICM Control Delay, s ICM LOS Minor Lane/Major Mvmt Capacity (veh/h) ICM Lane V/C Ratio ICM Control Delay (s) | 4.6 | EBL 1618 0.008 7.2 | EBT - - | WBT - | A WBR S | SBLn1 1074 0.039 8.5 | |
| Approach ICM Control Delay, s ICM LOS Minor Lane/Major Mvmt Capacity (veh/h) ICM Lane V/C Ratio ICM Control Delay (s) ICM Lane LOS | 4.6 | EBL 1618 0.008 7.2 A | EBT - - 0 A | WBT - - - | A WBR : | SBLn1 1074 0.039 8.5 Δ | |
| Approach ICM Control Delay, s ICM LOS Minor Lane/Major Mvmt Capacity (veh/h) ICM Lane V/C Ratio ICM Control Delay (s) ICM Lane LOS ICM Lane LOS | 4.6 | EBL 1618 0.008 7.2 A 0 | EBT - 0 A | WBT - - - | A WBR S | <u>5BLn1</u> 1074 0.039 8.5 A 0 1 | |

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| 0. 01/ 200 0. 00 | CCI 2 | | | | | | |
|------------------------|--------|--|-----------|------|--------|-------|--|
| Intersection | | | | | | | |
| Int Delay, s/veh | 4 | | | | | | |
| Movement | EBI | EBT | W/RT | MRR | SBI | CRP | |
| ane Configurations | EDL | CDT A | 1 | WDI | ODL | ODI | |
| Traffic Vol. veh/h | 13 | 17 | 39 | 1 | 7 | 38 | |
| Future Vol. veh/h | 13 | 17 | 39 | 1 | 2 | 38 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Free | Free | Free | Free | Stop | Stop | |
| RT Channelized | - | None | - | None | | None | |
| Storage Length | - | - | - | - | 0 | - | |
| Veh in Median Storage | .,# - | 0 | 0 | - | 0 | - | |
| Grade, % | | 0 | 0 | - | 0 | | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Nvmt Flow | 14 | 18 | 42 | 1 | 2 | 41 | |
| Major/Minor | Major1 | 1 | Major2 | | Minor2 | | |
| Conflicting Flow All | 43 | 0 | 1141012 | 0 | 89 | 43 | |
| Stage 1 | - | - | - | - | 43 | - | |
| Stage 2 | - | 1000 1000 1000 1000 1000 1000 1000 100 | - | - | 46 | - | |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 | |
| Critical Hdwy Stg 1 | | | - | - | 5.42 | - | |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - | |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 | |
| Pot Cap-1 Maneuver | 1566 | - | - | - | 912 | 1027 | |
| Stage 1 | - | - | - | - | 979 | - | |
| Stage 2 | - | - | - | - | 976 | - | |
| Platoon blocked, % | 4500 | - | - | - | 204 | 4007 | |
| Nov Cap-1 Maneuver | 1500 | - | | - | 904 | 1027 | |
| Nov Cap-2 Maneuver | - | - | - | | 904 | - | |
| Stage 2 | | - | CHERON IN | | 976 | No. | |
| Oldys 2 | | | | | 310 | | |
| Approach | EB | | WB | | SB | | |
| HCM Control Delay, s | 3.2 | | 0 | | 8.7 | | |
| HCM LOS | | | | | A | | |
| | | | | | | | |
| Minor Lane/Major Mvm | 1 | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | | 1566 | - | - | - | 1020 | |
| CM Lane V/C Ratio | | 0.009 | - | - | - | 0.043 | |
| ICM Control Delay (s) | | 1.3 | 0 | - | - | 8.7 | |
| 1CM Lane LUS | | A | A | - | - | A | |
| | | No. Com | | | | **** | |

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| 4: CR 206 & St | reet 3 | i | | | | | AM 2021 Site + Non-Site |
|------------------------|----------|-------|--------------------|------|----------|--------|-------------------------|
| Intersection | | | | | | | |
| Int Delay, s/veh | 2.8 | | | | | | |
| Movement | ERI | ERT | MOT | MPD | CDI | CDD | |
| Lane Configurations | EDL | EDI | The state | WBR | SDL | ODK | |
| Traffic Vol. veh/h | 13 | 28 | 76 | 1 | ·T' 2 | 37 | |
| Future Vol. veh/h | 13 | 28 | 76 | 1 | 2 | 37 | |
| Conflicting Peds. #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Free | Free | Free | Free | Stop | Stop | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | - | - | - | - | 0 | - | |
| Veh in Median Storage | ə,# - | 0 | 0 | - | 0 | - | |
| Grade, % | - | 0 | 0 | - | 0 | - | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Mvmt Flow | 14 | 30 | 83 | 1 | 2 | 40 | |
| | | | | | | | |
| Major/Minor | Major1 | ſ | Major2 | ľ | Minor2 | | |
| Conflicting Flow All | 84 | 0 | - | 0 | 142 | 84 | |
| Stage 1 | - | - | - | - | 84 | - | |
| Stage 2 | - | - | - | - | 58 | - | |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 | |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - | |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - | |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 | |
| Pot Cap-1 Maneuver | 1513 | - | - | - | 851 | 975 | |
| Stage 1 | - | - | - | - | 939 | - | |
| Stage 2 | | - | | | 905 | - | |
| May Cap 1 Maneuver | 1513 | | | - | 8/3 | 075 | |
| Mov Cap-2 Maneuver | - | - | - | | 843 | 910 | |
| Stage 1 | - | - | | | 931 | | |
| Stage 2 | - | - | - | - | 965 | - | |
| | | | | | | | |
| Approach | EB | | WB | | SB | | |
| HCM Control Delay, s | 2.3 | | 0 | | 8.9 | | |
| HCMLOS | | | and a state of the | | A | | |
| | | | | | | | |
| Minor Lane/Major Mym | at | EBI | FBT | WBT | WBR | SBI n1 | |
| Capacity (veh/h) | <u>a</u> | 1513 | | - | - VUDICE | 967 | |
| HCM Lane V/C Ratio | | 0.009 | - | | - | 0 044 | |
| -ICM Control Delay (s) | | 7.4 | 0 | - | - | 8.9 | |
| -ICM Lane LOS | | A | A | - | - | A | |
| -ICM 95th %tile Q(veh) | | 0 | - | - | - | 0.1 | |
| | | | | | | | |

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| Intersection Int Delay, s/veh Lane Configurations Fraffic Vol, veh/h Future Vol, veh/h Sonflicting Peds, #/hr Sign Control Si RT Channelized Storage Length | 2.5 VBL | | | | | | |
|---|------------|-------|--------|--------------------|--------------|------|--|
| nt Delay, s/veh nt Delay, s/veh <u>Movement</u> Ware Configurations [raffic Vol, veh/h -uture Vol, veh/h -onflicting Peds, #/hr Sign Control Str Channelized Storage Length | 2.5 VBL | MDD | | Contraction of the | | | |
| Avernent W ane Configurations 'raffic Vol, veh/h 'uture Vol, veh/h Jonflicting Peds, #/hr Sign Control SI RT Channelized Storage Length | VBL W | MDD | | | | | |
| ane Configurations Traffic Vol, veh/h Tuture Vol, veh/h Conflicting Peds, #/hr Sign Control Si ≷T Channelized Xorage Length | Y | VVDI | NBT | NBR | SBL | SBT | |
| Traffic Vol, veh/h Future Vol, veh/h Conflicting Peds, #/hr Sign Control SI रT Channelized Storage Length | 100 | | P | | | र्स | |
| Future Vol, veh/h Conflicting Peds, #/hr Sign Control Si RT Channelized Storage Length | 72 | 6 | 95 | 121 | 8 | 46 | |
| Conflicting Peds, #/hr Sign Control Si RT Channelized Storage Length | 72 | 6 | 95 | 121 | 8 | 46 | |
| Sign Control S RT Channelized Storage Length | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Length | Stop | Stop | Free | Free | Free | Free | |
| Storage Lengui | - | None | - | None | - | None | |
| /eb in Median Storage # | 10 | | 0 | | <u> </u> | 0 | |
| Grade. % | 0 | - | 0 | Allowing . | | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| leavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| /lvmt Flow | 78 | 7 | 103 | 132 | 9 | 50 | |
| | | | | | | | |
| Major/Minor Mino | nor1 | N | Major1 | | Major2 | | |
| Conflicting Flow All 2 | 237 | 169 | 0 | 0 | 235 | 0 | |
| Stage 1 1 | 169 | - 1 | • | - | - | - | |
| Stage 2 | 68 | - 00 | - | - | - | - | |
| Critical Howy b. | 5.42 | 6.22 | • | - | 4.12 | - | |
| Titical Hdwy Stg 7 5. | 5.42 | - | | | - | - | |
| Follow-up Hdwy 3.5 | 518 | 3 318 | | Anna a | 2,218 | - | |
| ot Cap-1 Maneuver 7 | 751 | 875 | | - | 1332 | - | |
| Stage 1 8 | 861 | - | - | - | - | - | |
| Stage 2 9 | 955 | - | - | - | - | - | |
| latoon blocked, % | | | - | - | 1300 | - | |
| Nov Cap-1 Maneuver / | 746 | 875 | - | - | 1332 | - | |
| Nov Cap-2 Maneuver 7 | 740 | | - | - | - | - | |
| Stage 2 9 | 955 | | - | | and a second | - | |
| olugo z | 500 | | | | | | |
| lonroach l | W/R | | NB | | SB | | |
| ICM Control Delay s 1(| 10.4 | | 0 | | 11 | | |
| ICM LOS | B | | U | | 1.1 | | |
| | | | | | | | |
| /inor Lane/Major Mymt | | NBT | NBRV | VBI n1 | SBL | SBT | |
| Canacity (veh/h) | | - | - | 755 | 1332 | - | |
| 1CM Lane V/C Ratio | | - | - | 0.112 | 0.007 | - | |
| ICM Control Delay (s) | | - | - | 10.4 | 7.7 | 0 | |
| ICM Lane LOS | | - | - | В | А | А | |
| ICM 95th %tile Q(veh) | | - | - | 0.4 | 0 | - | |
| | | | | | | 2 | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 32 of 59 October 12, 2020

| Den ande 25 en des gewannen der Stellung in den die Gescher Berner Berner von der Staten ander der Berner von B |
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Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 33 of 59 October 12, 2020

| . 011200 0.00 | reet 2 | | | | | | PM 2021 Site + Non-Site |
|--|----------|---------------------------------|---------------------------|--------------------|---------------------------|-----------------------------------|-------------------------|
| ntersection | | | | | | | |
| Int Delay, s/veh | 3.8 | and the state | | | | | |
| Movement | EDI | EDT | MOT | MIDD | CDI | CDD | |
| Long Configurations | EBL | EBI | WBI | WBR | SBL | SBR | |
| | 13 | 45 | 30 | 2 | T. 2 | 26 | |
| Future Vol. veh/h | 43 | 45 | 30 | 2 | 2 | 20 | |
| Conflicting Peds. #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Free | Free | Free | Free | Stop | Stop | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | - | - | - | - | 0 | | |
| Veh in Median Storage | ,# - | 0 | 0 | - | 0 | - | |
| Grade, % | - | 0 | 0 | - | 0 | 2. | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Mvmt Flow | 47 | 49 | 33 | 2 | 2 | 28 | |
| | | | | | | | |
| Major/Minor I | Major1 | ٨ | Major2 | 1 | Minor2 | | |
| Conflicting Flow All | 35 | 0 | - | 0 | 177 | 34 | |
| Stage 1 | - | • | - | - | 34 | - | |
| Stage 2 | - | - | - | - | 143 | - | |
| Critical Hdwy | 4.12 | - | + | - | 6.42 | 6.22 | |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - | |
| Critical Howy Stg 2 | - | - | - | - | 5.42 | - | |
| Pollow-up Huwy | 1576 | - | - | - | 3.518 | 3.318 | |
| Stane 1 | 1370 | | - | | 013 | 1039 | |
| Stage 2 | - | | | - | 884 | | |
| Platoon blocked, % | | - | - | - | 001 | | |
| Mov Cap-1 Maneuver | 1576 | - | - | - | 788 | 1039 | |
| Mov Cap-2 Maneuver | - | - | - | - | 788 | - | |
| Stage 1 | - | - | - | - | 957 | - | |
| Stage 2 | - | - | - | - | 884 | | |
| | | | | | | | |
| | EB | | WB | | SB | | |
| Approach | 26 | S. Sa | 0 | | 8.7 | | |
| Approach HCM Control Delay, s | 5.0 | | | | ٨ | | |
| Approach HCM Control Delay, s HCM LOS | 5.0 | | | | A | | |
| Approach HCM Control Delay, s HCM LOS | 3.0 | | | | A | | |
| Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm | 3.0 t | EBL | EBT | WBT | WBR | SBLn1 | |
| Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) | 5.0 t | EBL 1576 | EBT | WBT | WBR | SBLn1 1016 | |
| Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio | 3.0 t | EBL 1576 0.03 | EBT - | WBT - | WBR | 5BLn1 1016 0.03 | |
| Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) | t | EBL 1576 0.03 7.4 | <u>EBT</u> - - 0 | WBT - - | WBR | SBLn1 1016 0.03 8.7 | |
| Approach HCM Control Delay, s HCM LOS Vinor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) HCM Lane LOS | t | EBL 1576 0.03 7.4 A | EBT - - 0 A | WBT - - - | A WBR : - - - | SBLn1 1016 0.03 8.7 A | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 34 of 59 October 12, 2020

| 4: CK 200 & 31 | reet a | , | | | | | PM 2021 Site + Non-Site |
|------------------------|-------------|------|----------|------|---------------------------|-------|-------------------------|
| 1 | | | | | | | |
| ntersection | 25 | | | | | | |
| nt Delay, s/ven | 2.5 | | | | | | |
| Novement | EBL | EBT | WBT | WBR | SBL | SBR | |
| ane Configurations | | é. | Ъ | | W | | |
| Traffic Vol, veh/h | 42 | 87 | 54 | 2 | 1 | 24 | |
| Future Vol, veh/h | 42 | 87 | 54 | 2 | 1 | 24 | |
| Conflicting Peas, #/nr | 0 | U | 0 | 0 | 0 Chan | 0 | |
| Sign Control | Free | Free | Free | Free | Stop | Stop | |
| Storage Length | | None | | None | 0 | None | |
| leh in Median Storage | e# - | 0 | 0 | | 0 | | |
| Grade. % | - | 0 | 0 | - | 0 | - | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| leavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Nvmt Flow | 46 | 95 | 59 | 2 | 1 | 26 | |
| | | | | | | | |
| Major/Minor | Major1 | 1 | Major2 | 1 | Minor2 | | |
| Conflicting Flow All | 61 | 0 | najorz - | 0 | 247 | 60 | |
| Stage 1 | - | - | | - | 60 | - | |
| Stage 2 | - | - | - | - | 187 | - | |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 | |
| Critical Hdwy Stg 1 | -Europerson | | | - | 5.42 | | |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - | |
| Follow-up Hdwy | 2.218 | | | - | 3.518 | 3.318 | |
| Pot Cap-1 Maneuver | 1542 | - | - | - | 741 | 1005 | |
| Stage 1 | - | - | | • | 963 | - | |
| Stage 2 | - | - | - | - | 845 | - | |
| Platoon blocked, % | 4540 | - | - | - | 740 | 4005 | |
| Nov Cap-1 Waneuver | 1542 | | | | 718 | 1005 | |
| Stage 1 | | | - | - | 933 | - | |
| Stage 2 | | - | - | | 845 | - | |
| oluge _ | | | | | 040 | | |
| A | CD. | | MID | | 00 | | |
| Approach | 24 | | WB | | 0.7 | | |
| HCM Control Delay, S | 2.4 | | 0 | | 8.7 | | |
| | | | | | A | | |
| | | | | | Contraction of the second | | |
| Minor Lane/Major Mvm | it | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | | 1542 | - | - | - | 989 | |
| ICM Lane V/C Ratio | | 0.03 | - | | - | 0.027 | |
| ICM Control Delay (s) | | 7.4 | 0 | - | - | 8.7 | |
| CM Lane LUS | | A | A | - | - | A | |
| TON Sour Whe given | 1 | 0.1 | - | | - | 0.1 | |
| | | | | | | | |

Appendix C2

2025 AM & PM Traffic Conditions with 100 % Development

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 36 of 59 October 12, 2020

| Intersection Int Delay, s/veh Movement V Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Conflicting Peds, #/hr Sign Control S RT Channelized | 10 WBL 301 301 0 | WBR 21 21 | NBT | NBR | SBL | SBT | |
|--|---|-----------------|--------|--------|--------|-----------|--|
| Intersection Int Delay, s/veh Movement V Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Conflicting Peds, #/hr Sign Control S RT Channelized | 10 WBL ¥ 301 301 0 | WBR 21 21 | NBT | NBR | SBL | SBT | |
| Movement V Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Conflicting Peds, #/hr Sign Control S RT Channelized | NBL WBL 301 301 301 0 | WBR 21 21 | NBT | NBR | SBL | SBT | |
| Movement V Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Conflicting Peds, #/hr Sign Control S RT Channelized | VBL 301 301 0 | 21 | NBT | NBR | SBL | SBT | |
| Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Conflicting Peds, #/hr Sign Control S RT Channelized | 301 301 0 | 21 | 103 | | | | |
| l raffic Vol, ven/h Future Vol, veh/h Conflicting Peds, #/hr Sign Control S RT Channelized | 301 301 0 | 21 | 103 | | 10 | 4 | |
| Conflicting Peds, #/hr Sign Control S RT Channelized | 0 | | 100 | 105 | 18 | 299 | |
| Sign Control S RT Channelized | U | 0 | 103 | 105 | 18 | 299 | |
| RT Channelized | Stop | Stop | Free | Free | Free | Free | |
| | - | None | - | None | - | None | |
| Storage Length | 0 | - | - | - | - | - | |
| Veh in Median Storage, # | ŧ 0 | - | 0 | - | - | 0 | |
| Grade, % | 0 | - | 0 | - | - | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Venicles, % | 2 2 2 2 2 | 2 | 2 | 2 | 2 | 2 | |
| WINTER FIOW | 321 | 23 | 112 | 114 | 20 | 325 | |
| | - | | | | | | |
| Major/Minor Mir | nor1 | ١ | Major1 | | Major2 | | |
| Conflicting Flow All | 534 | 169 | 0 | 0 | 226 | 0 | |
| Stage 1 | 169 | - | - | - | - | - | |
| Critical Hdway | 6.42 | 6.22 | • | - | 4 12 | - | |
| Critical Hdwy Sto 1 | 5 42 | 0.22 | - | - | 4.12 | - | |
| Critical Hdwy Stg 2 5 | 5.42 | | - | | - | - | |
| Follow-up Hdwy 3. | 518 | 3.318 | - | - | 2.218 | - | |
| Pot Cap-1 Maneuver | 507 | 875 | - | - | 1342 | - | |
| Stage 1 | 861 | - | • | - | - | | |
| Stage 2 | 702 | - | - | - | - | - | |
| Platoon blocked, % | 100 | 075 | - | - | 4040 | - | |
| Nov Cap-1 Maneuver | 498 | 8/5 | - | - | 1342 | - | |
| Stage 1 | 846 | | | | | | |
| Stage 2 | 702 | - | - | - | - | - | |
| | | | | | | | |
| oproach | M/R | | NB | | SB | | |
| ICM Control Delay s 2 | 25.9 | | | | 0.4 | | |
| ICM LOS | D | | U | | 0.4 | | |
| | | | | | | | |
| liner Lang/Major Mumt | | NIDT | NIDDW | /DI n4 | ODI | OPT | |
| Capacity (veh/h) | | INDI | INDIN | 512 | 1242 | JDI | |
| CM Lane V/C Ratio | | | | 0 684 | 0.015 | - | |
| ICM Control Delay (s) | | - | | 25.9 | 7.7 | 0 | |
| | | - | - | D | A | A | |
| ICM Lane LOS | | | | | 0 | ann an tr | |
| ICM Lane LOS ICM 95th %tile Q(veh) | | - | - | 5.2 | U | | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 37 of 59 October 12, 2020

| | 1001 | | | | | | Aivi 2020 Site + NOT-Site |
|--|-----------|----------------------------------|-------------------------------|--------------------|--|------------------------------------|---------------------------|
| | | | | | | | |
| Intersection | | | | | | | |
| Int Delay, s/veh | 6.9 | | | | | | |
| Movement | FRI | FRT | WRT | WRR | SBI | SBR | |
| Lane Configurations | | 4 | 1 | WDIX | N/ | ODIT | |
| Traffic Vol. veh/h | 36 | 27 | 5 | 2 | 6 | 107 | |
| Future Vol, veh/h | 36 | 27 | 5 | 2 | 6 | 107 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Free | Free | Free | Free | Stop | Stop | |
| RT Channelized | - | None | | None | - | None | |
| Storage Length | - | - | - | | 0 | - | |
| Veh in Median Storage | e,# - | 0 | 0 | - | 0 | - | |
| Grade, % | - | 0 | 0 | - | 0 | - | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| neavy venicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| www.internow | 39 | 29 | 5 | 2 | 1 | 116 | |
| | | | | | All Manuference | | |
| Major/Minor | Major1 | A N | Aajor2 | 1 | Ainor2 | | |
| Conflicting Flow All | 7 | 0 | - | 0 | 113 | 6 | |
| Stage 1 | - | - 1 | - | - | 6 | - | |
| Stage 2 | - | - | - | - | 107 | - | |
| Critical Hdwy | 4.12 | | - | - | 6.42 | 6.22 | |
| Critical Howy Stg 1 | - | - | - | - | 5.42 | - | |
| Enllow-up Hdwy | 2 218 | 1821.2. - 1 | • | - | 2.510 | 2 210 | |
| Pot Can-1 Maneuver | 1614 | | - | | 884 | 1077 | |
| Stage 1 | - | - | - | - | 1017 | - | |
| Stage 2 | - | - | - | - | 917 | - | |
| Platoon blocked, % | | - | - | - | | | |
| Mov Cap-1 Maneuver | 1614 | - | - | - | 862 | 1077 | |
| Mov Cap-2 Maneuver | - | | - | - | 862 | - | |
| A . 1 | - | - | - | - | 992 | - | |
| Stage 1 | | - | - | - | 917 | - | |
| Stage 1 Stage 2 | - | | | | | | |
| Stage 1 Stage 2 | - | | | | | | |
| Stage 1 Stage 2 Approach | EB | | WB | | SB | | |
| Stage 1 Stage 2 Approach HCM Control Delay, s | EB 4.2 | | WB 0 | | SB 8.8 | | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS | EB 4.2 | | WB 0 | | SB 8.8 A | | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS | EB 4.2 | | WB 0 | | SB 8.8 A | | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Maior Mvm | EB 4.2 | EBL | WB 0 EBT | WBT | SB 8.8 A WBR | SBLn1 | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) | EB 4.2 | EBL 1614 | WB 0 EBT | WBT | SB 8.8 A WBR | SBLn1 1063 | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio | EB 4.2 | EBL 1614 0.024 | WB 0 EBT | WBT - | SB 8.8 A WBR | SBLn1 1063 0.116 | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) | EB 4.2 | EBL 1614 0.024 7.3 | WB 0 EBT - 0 | WBT - - | SB 8.8 A WBR | SBLn1 1063 0.116 8.8 | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) HCM Lane LOS | EB 4.2 | EBL 1614 0.024 7.3 A | WB 0 EBT - 0 A | WBT - - - | SB 8.8 A WBR : - - - | SBLn1 1063 0.116 8.8 A | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 38 of 59 October 12, 2020

| 3: UK 200 & 31 | reet z | <u> </u> | | | | | Aivi 2023 Site + Nori-Site |
|------------------------|-----------|----------|--------|------|--------|-------|----------------------------|
| | | | | | | | |
| Intersection | | | | | | | |
| Int Delay, s/veh | 4.2 | | | | | | |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR | |
| Lane Configurations | to to be | el la | L | WEIT | W | ODIT | |
| Traffic Vol, veh/h | 36 | 57 | 110 | 2 | 6 | 107 | |
| Future Vol, veh/h | 36 | 57 | 110 | 2 | 6 | 107 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Free | Free | Free | Free | Stop | Stop | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | - # | - | - | - | 0 | - | |
| Ven in Median Storage | 9,77 - | 0 | 0 | | 0 | - | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Mvmt Flow | 39 | 62 | 120 | 2 | 7 | 116 | |
| | | | | | | | |
| Major/Minor | Major1 | 1 | Major2 | 1 | Minor2 | | |
| Conflicting Flow All | 122 | 0 | - | 0 | 261 | 121 | |
| Stage 1 | - | - | - | - | 121 | | |
| Stage 2 | - | - | - | - | 140 | - | |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 | |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - | |
| Critical Hdwy Stg 2 | - 0.040 | - | - | - | 5.42 | - | |
| Pollow-up Howy | 2.218 | - | - | - | 3.518 | 3.318 | |
| Stage 1 | 1400 | - | - | - | 904 | 950 | |
| Stage 2 | - | - | - | - | 887 | - | |
| Platoon blocked, % | | - | - | | | | |
| Mov Cap-1 Maneuver | 1465 | - | - | - | 708 | 930 | |
| Mov Cap-2 Maneuver | - | - | • | | 708 | - | |
| Stage 1 | - | - | - | - | 879 | - | |
| Stage 2 | - | - | - | - | 887 | - | |
| | | | | | | | |
| Approach | EB | | WB | | SB | | |
| HCM Control Delay, s | 2.9 | | 0 | | 9.5 | | |
| 1CM LOS | | | | | A | | |
| | | | | | | | |
| Minor Lane/Major MVm | <u>it</u> | EBL | EBI | WBI | WBR 3 | SBLn1 | |
| Capacity (Ven/n) | | 1400 | | | | 910 | |
| HCM Control Delay (s) | | 7.5 | 0 | - | | 9.5 | |
| HCM Lane LOS | | A | A | | - | A | |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | - | 0.5 | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | 1 | | | | | | |
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Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 39 of 59 October 12, 2020

| | | 4 - Marca 1944 | | | | | |
|------------------------|-----------|----------------|-----------|-----------|--------|----------------|--|
| ntersection | | | | | 1000 | | |
| nt Delay, s/veh | 3.2 | | | | | | |
| Novement | EBL | EBT | WBT | WBR | SBL | SBR | |
| ane Configurations | | ર્લ | Þ | | Y | | |
| raffic Vol, veh/h | 36 | 87 | 215 | 2 | 6 | 107 | |
| Future Vol, veh/h | 36 | 87 | 215 | 2 | 6 | 107 | |
| Conflicting Peds, #/nr | 0 Eroo | U | 0 Eroo | 0 Eroo | O | 0 Ctop | |
| RT Channelized | Fiee - | None | Fiee - | None | Stop | None | |
| Storage Length | - | - | - | - | 0 | - | |
| eh in Median Storage | ,# - | 0 | 0 | - | 0 | | |
| Grade, % | | 0 | 0 | - | 0 | - | <u>24 millionaria (1997) a posta de la constancia d</u> |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| leavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| ivmt Flow | 39 | 95 | 234 | 2 | 1 | 116 | |
| Jaior/Minor | laior1 | N | Jaior? | | linor? | and the second | |
| Conflicting Flow All | 236 | 0 | najuiz | 0 | 408 | 235 | |
| Stage 1 | - | - | - | - | 235 | - | |
| Stage 2 | - | - | - | - | 173 | - | |
| critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 | |
| ritical Hdwy Stg 1 | | - | - | - | 5.42 | - | |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - | |
| ollow-up Howy | 1331 | - | | - | 3.518 | 3.318 | |
| Stage 1 | 1001 | - | - | - | 804 | 004 | |
| Stage 2 | - | - | - | - | 857 | - | |
| latoon blocked, % | | | - | - | | | |
| lov Cap-1 Maneuver | 1331 | - | - | - | 580 | 804 | |
| lov Cap-2 Maneuver | - | - | - | - | 580 | - | |
| Stage 1 | - | - | 1 | - | 957 | - | |
| Oldge 2 | | | - | | 037 | | |
| pproach | EB | | WB | | SB | | |
| CM Control Delay, s | 2.3 | | 0 | | 10.4 | | |
| ICM LOS | | | | | В | | |
| | | | | | | | |
| linor Lane/Major Mvm | t | EBL | EBT | WBT | WBR | SBLn1 | |
| apacity (veh/h) | | 1331 | - | - | - | 788 | |
| CM Control Delay (c) | | 7.8 | - | - | - | 10.156 | |
| CM Lane LOS | | A | A | - - | - | B | |
| CM 95th %tile Q(veh) | | 0.1 | - | - | - | 0.6 | |
| | | | | | | | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 40 of 59 October 12, 2020

| 11: FM 543 & S | street | 4 | an succession of the succession of the | and a second state of the | | | AM 2025 Site + Non-Site |
|------------------------|--------|---------------|--|---|--------------|-------|-------------------------|
| | | | | | | | |
| ntersection | | | | | | | |
| Int Delay, s/veh | 2.3 | | | | - | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | |
| Lane Configurations | W | | () | | | ર્લ | |
| Traffic Vol, veh/h | 81 | 4 | 98 | 26 | 2 | 236 | |
| Future Vol, veh/h | 81 | 4 | 98 | 26 | 2 | 236 | |
| Conflicting Peds, #/hr | U Chan | U | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| Storage Length | 0 | None - | - | None - | | NUII0 | |
| Veh in Median Storage | .# 0 | - | 0 | - | - | 0 | |
| Grade, % | 0 | - | 0 | - | - | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| MVmt Flow | 88 | 4 | 107 | 28 | 2 | 257 | |
| | | | | | | | |
| Major/Minor M | Minor1 | I | Major1 | | Major2 | | |
| Conflicting Flow All | 382 | 121 | 0 | 0 | 135 | 0 | |
| Stage 1 | 121 | | | - | - | - | |
| Critical Hdwy | 6.42 | 6.22 | | - | 4 12 | | |
| Critical Hdwy Stg 1 | 5.42 | 0.22 | - | - | 4.14 | - | |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - | |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - | |
| Pot Cap-1 Maneuver | 620 | 930 | - | - | 1449 | - | |
| Stage 1 | 904 | - | - | - | - | - | |
| Stage 2 | 183 | - | - | - | - | - | |
| Mov Cap-1 Maneuver | 619 | 930 | | - | 1449 | - | |
| Nov Cap-2 Maneuver | 619 | | - | - | - | - | |
| Stage 1 | 902 | - | - | - | - | - | |
| Stage 2 | 783 | - | - | - | - | | |
| | | | | | | | |
| Approach | WB | | NB | | SB | | |
| HCM Control Delay, s | 11.7 | | 0 | | 0.1 | | |
| HCM LOS | В | | | | | | |
| | | 22000 | | | | | |
| Minor Lane/Major Mvm | t | NBT | NBRV | VBLn1 | SBL | SBT | |
| Capacity (veh/h) | | - | - | 629 | 1449 | - | |
| -ICM Lane V/C Ratio | | - | - | 0.147 | 0.002 | - | |
| HCM Lane LOS | | Alline | - | B | 7.5 A | A | |
| ICM 95th %tile Q(veh) | | - | - | 0.5 | 0 | - | |
| | | | | All the Case of the | Allastration | | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 41 of 59 October 12, 2020

| 13: FM 543 & S | treet | 5 | | | | | AM 2025 Site + Non-Site |
|------------------------|-----------|-------|-------------|--------|--------|--------------|-------------------------|
| | | | | | | | |
| ntersection | 1.0 | | | | | | |
| nt Delay, s/ven | 1.8 | | | | | | |
| Novement | WBL | WBR | NBT | NBR | SBL | SBT | |
| ane Configurations | 50 | | 1 * | 40 | | ا | |
| Future Vol. veh/h | 53 | 4 | 84 | 18 | 1 | 185 | |
| Conflicting Peds. #/hr | 0 | 4 | 04 | 0 | 0 | 0 | |
| Sian Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | - | None | | None | - | None | |
| Storage Length | 0 | - | - | - | - | - | |
| Veh in Median Storage | ,# 0 | - | 0 | - | - | 0 | |
| Grade, % | 0 | - | 0 | - | - | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Mumt Flow | 58 | 4 | 91 | 20 | 1 | 201 | |
| WWITH FIOW | 00 | | 01 | 20 | | 201 | |
| Major/Minor | Ainor1 | 1 | Majort | | Major? | | |
| Conflicting Flow All | 304 | 101 | 0 | 0 | 111 | 0 | |
| Stage 1 | 101 | - | - | - | - | - | |
| Stage 2 | 203 | - | - | - | - | - | |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - | |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | | |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - | |
| Follow-up Hawy | 3.518 | 3.318 | - NUMBER | - | 2.218 | - | |
| Stage 1 | 923 | 904 | | | 1419 | - | |
| Stage 2 | 831 | - | - | - | - | - | |
| Platoon blocked, % | | | . | | | - | |
| Mov Cap-1 Maneuver | 687 | 954 | - | - | 1479 | - | |
| Mov Cap-2 Maneuver | 687 | - | - | - | - | - | |
| Stage 1 | 922 | | - | - | - | - | |
| Stage 2 | 831 | - | - | - | - | - | |
| A | MD | | ND | | 00 | | |
| Approach | 10.6 | | NB | | 0 | | |
| HCMLOS | 10.0 B | | 0 | | 0 | | |
| | 5 | | | | | | |
| Minor Lane/Major Mym | ŧ | NBT | NBRV | VBL n1 | SBI | SBT | |
| Canacity (veh/h) | | - | - | 701 | 1479 | - | |
| HCM Lane V/C Ratio | | - | - | 0.088 | 0.001 | - | |
| HCM Control Delay (s) | | - | - | 10.6 | 7.4 | 0 | |
| ICM Lane LOS | | - | - | В | А | А | |
| ICM 95th %tile Q(veh) | | - | - | 0.3 | 0 | - | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 42 of 59 October 12, 2020

| 15: FIM 543 & 5 | treet | 6 | | - | | | AM 2025 Site + Non-Site |
|--------------------------------|--------|------------|------------|-----------|--------|-----------|-------------------------|
| | | | | | | | |
| ntersection | 1000 | | enter 1 | | | | |
| nt Delay, s/veh | 3.1 | | | | | | |
| Novement | WBL | WBR | NBT | NBR | SBL | SBT | |
| ane Configurations | Y | | <u>a</u> | | | Â | |
| raffic Vol, veh/h | 81 | 4 | 62 | 26 | 2 | 105 | |
| future Vol, veh/h | 81 | 4 | 62 | 26 | 2 | 105 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | 0 | - | - | - | - | - | |
| /eh in Median Storage | ,# 0 | - | 0 | - | - | 0 | |
| Grade, % | 0 | - | 0 | - | - | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| leavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Avmt Flow | 88 | 4 | 67 | 28 | 2 | 114 | |
| | | | | | | | |
| Major/Minor N | Minor1 | 1 | Major1 | 1 | Major2 | | |
| Conflicting Flow All | 199 | 81 | 0 | 0 | 95 | 0 | |
| Stage 1 | 81 | - | - | - | - | - | |
| Stage 2 | 118 | - | - | - | - | - | |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - | |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - | |
| ollow-up Hdwy | 3.518 | 3.318 | | | 2.218 | - | |
| ot Cap-1 Maneuver | 790 | 979 | - | - | 1499 | - | |
| Stage 1 | 942 | • | | - | • | - | |
| Stage 2 | 907 | • | - | - | - | • | |
| latoon blocked, % | | | - | - | | - | |
| Nov Cap-1 Maneuver | 789 | 979 | - | - | 1499 | - | |
| Nov Cap-2 Maneuver | 789 | - | - | - | - | - | |
| Stage 1 | 941 | - | - | • | - | - | |
| Stage 2 | 907 | - | - | - | - | - | |
| | | | | | | | |
| Approach | WB | 0.0 | NB | | SB | | |
| -ICM Control Delay, s | 10.1 | | 0 | | 0.1 | | |
| ICM LOS | В | | | | | | |
| | | | | | | | |
| Vinor Lane/Major Mymt | | MBT | NRRV | | SBI | PRT | |
| Consolity (ush/h) | | NDT | NERV | 706 | 1400 | 301 | |
| Capacity (venin) | | | | 190 | 1499 | 1000 | |
| 1CM Control Dolou (c) | | - | | 10.1 | 0.001 | - | |
| CML and LOS | | | | 10.1 D | 1.4 | 0 | |
| ICM Of the Wile O(veh) | | esonome | - | 0.4 | A | А | |
| The state of the second second | | AN ASSAULT | ASSESSED A | 0.4 | U | ALCONT OF | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 43 of 59 October 12, 2020

| 1: FM 543 & CI | R 206 | <u>;</u> | | | | | PM 2025 Site + Non-Site |
|---|------------------------|----------|--------|--------|---|---|-------------------------|
| Intersection | | | | | | | |
| nt Delay, s/veh | 7.9 | | | | | | |
| Novement | WBL | WBR | NBT | NBR | SBL | SBT | |
| ane Configurations | W | | P | | | 4 | |
| Fraffic Vol, veh/h | 205 | 26 | 337 | 344 | 27 | 186 | |
| Future Vol, veh/h | 205 | 26 | 337 | 344 | 27 | 186 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | • | None | - | None | - | None | |
| Storage Length | 0 | - | - | - | - | - | |
| /eh in Median Storage | e,# 0 | - | 0 | - | - | 0 | |
| Grade, % | 0 | - | 0 | - | - | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| leavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| vivmt Flow | 223 | 28 | 366 | 374 | 29 | 202 | |
| Vaior/Minor | Minor1 | I | Maior1 | 1 | Major2 | | |
| Conflicting Flow All | 813 | 553 | 0 | 0 | 740 | 0 | |
| Stage 1 | 553 | - | - | - | - | - | |
| Stage 2 | 260 | | | | Eliza Gato dan | | |
| Critical Hdwy | 6.42 | 6.22 | | | 4 12 | | |
| critical Hdwy Sta 1 | 5.42 | - | | | - | in the second second | |
| Critical Hdwy Stg 2 | 5.42 | - | | - | - | | |
| ollow-up Hdwy | 3.518 | 3.318 | - | - | 2,218 | MAR STRATTA | |
| Pot Cap-1 Maneuver | 348 | 533 | | | 867 | | |
| Stage 1 | 576 | - | - | - | - | - | |
| Stage 2 | 783 | - | - | - | - | - | |
| Platoon blocked, % | Constant of the second | | - | - | | - | |
| Nov Cap-1 Maneuver | 335 | 533 | - | - | 867 | - | |
| Nov Cap-2 Maneuver | 335 | - | - | - | - | - | |
| Stage 1 | 554 | - 1 | - | - | | - | |
| Stage 2 | 783 | - | | - | | - | |
| , i i i i i i i i i i i i i i i i i i i | | | | | | | |
| Approach | WB | | NB | | SB | | |
| ICM Control Delay, s | 37.5 | | 0 | | 1.2 | | |
| ICM LOS | E | | | | | | |
| Ainor Lane/Maior Myn | ot | NBT | NBRV | /BI n1 | SBI | SBT | |
| Capacity (veh/h) | n | - | - | 350 | 867 | | |
| -CM Lane V/C Ratio | | | | 0 717 | 0.034 | alestates - | |
| ICM Control Delay (s) | | | | 37.5 | 93 | 0 | |
| ICM Long LOS | | | | F | Δ | Δ | |
| | - | | - | E 2 | 0.1 | A | |
| CM 05th %tile O(veh) | 1.26.29 | | | | and the second se | and the second se | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 44 of 59 October 12, 2020

| 2: CR 206 & St | reet 1 | | | | | | PM 2025 Site + Non-Site |
|-----------------------|--------|-------|--------|------|--------|---------------------|-------------------------|
| | | | | | | | |
| Intersection | | | | | | guite de | |
| Int Delay, s/veh | 6.3 | | | | | | |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR | |
| Lane Configurations | | ર્લ | f, | | Y | 101 (110 M 200 PD M | |
| Traffic Vol, veh/h | 121 | 16 | 31 | 6 | 4 | 71 | |
| Future Vol, ven/n | 121 | 16 | 31 | 6 | 4 | /1 | |
| Sign Control | Free | Free | Free | Eree | Stop | Stop | |
| RT Channelized | - | None | - | None | otop - | None | |
| Storage Length | - | - | - | - | 0 | - | |
| Veh in Median Storage | e, # - | 0 | 0 | - | 0 | - | |
| Grade, % | - | 0 | 0 | - | 0 | - | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| wint flow | 132 | 17 | 34 | 1 | 4 | 11 | |
| M-1- (A.P. | 14-1-1 | | | | 41 | | |
| Conflicting Flow All | Major1 | N | najor2 | - | vinor2 | 20 | |
| Stage 1 | 41 | U | - | U | 319 | 38 | |
| Stage 2 | | - | - | - | 281 | - | |
| Critical Hdwv | 4.12 | - | | - | 6.42 | 6.22 | |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | | |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - | |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 | |
| Pot Cap-1 Maneuver | 1568 | - | - | - | 674 | 1034 | |
| Stage 1 | | - | | - | 984 | - | |
| Stage 2 | - | - | • | - | 767 | - | |
| ration blocked, % | 1500 | - | - | - | 047 | 1004 | |
| Mov Cap-1 Maneuver | 1008 | - | • | - | 617 | 1034 | |
| Stage 1 | - | | - | | 900 | - | |
| Stage 2 | - | - | - | - | 767 | - | |
| . | | | | | | | |
| Approach | EB | | WB | | SB | | |
| HCM Control Delay, s | 6.6 | | 0 | | 8.9 | | |
| HCM LOS | | | | | А | | |
| | | | | | | | |
| Minor Lane/Major Mvm | it | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | | 1568 | - | - | - | 998 | |
| ICM Lane V/C Ratio | | 0.084 | - | - | - | 0.082 | |
| HCM Control Delay (s) | | 7.5 | 0 | - | - | 8.9 | |
| HOM Lane LOS | | A | A | - | - | A | |
| Now Som Whe Q(ven) | | 0.3 | - | - | - | 0.3 | |
| | | | | | | | × |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | _ | | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 45 of 59 October 12, 2020

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 46 of 59 October 12, 2020

| L.L | | | | | | | |
|-----------------------|---------------|-------|--------|------|------------|--------------------|--|
| Intersection | 2.0 | | | | | Alternation of the | |
| in Delay, s/ven | 2.0 | _ | | | | | |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR | |
| Lane Configurations | 404 | e | P | 0 | Y | 74 | |
| Traffic Vol, ven/h | 121 | 250 | 161 | 6 | 4 | /1 | |
| Conflicting Pede #/hr | 121 | 250 | 101 | 0 | 4 | /1 | |
| Sign Control | Free | Free | Free | Free | Stop | Stop | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | - | | - | - | 0 | - | |
| Veh in Median Storage | e, # - | 0 | 0 | - | 0 | - | |
| Grade, % | - | 0 | 0 | - | 0 | - | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| wint flow | 132 | 212 | 175 | 7 | 4 | 77 | |
| Maior/Minor | Major1 | N | Major2 | N | Ainor? | | |
| Conflicting Flow All | 182 | 0 | - | 0 | 715 | 179 | |
| Stage 1 | | - | - | - | 179 | - | |
| Stage 2 | - | - | - | - | 536 | - | |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 | |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - | |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - | |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 | |
| Stage 1 | 1393 | • | - | | 39/ | 864 | |
| Stage 2 | - | - | - | - | 002 587 | - | |
| Platoon blocked. % | WILL BE STATE | - | - | - | 001 | | |
| Mov Cap-1 Maneuver | 1393 | - | - | - | 353 | 864 | |
| Nov Cap-2 Maneuver | - | - | 37 | - | 353 | - | |
| Stage 1 | - | - | - | - | 757 | - | |
| Stage 2 | - | - | | - | 587 | - | |
| | | | | | | | |
| Approach | EB | | WB | | SB | | |
| HCM LOS | 2.0 | | U | | B | | |
| Minor Lane/Major Mvm | nt | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | | 1393 | - | | - | 802 | |
| HCM Lane V/C Ratio | | 0.094 | - | | - | 0.102 | |
| HCM Control Delay (s) | | 7.9 | 0 | - | - | 10 | |
| HCM Lane LOS | | A | A | - | - | B | |
| Jow Sour Wile Q(ven) | | 0.3 | - | | - | 0.3 | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 47 of 59 October 12, 2020

| | lieet | 4 | | | | | PM 2025 Site + Non-Site |
|------------------------|--------|------------|---------|-------------------|----------|------|-------------------------|
| Intersection | | | | | | | |
| Int Delay, s/veh | 1.3 | | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | |
| Lane Configurations | W | | 1. | | | લી | |
| Traffic Vol, veh/h | 53 | 3 | 272 | 91 | 5 | 160 | |
| Future Vol, veh/h | 53 | 3 | 272 | 91 | 5 | 160 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | 0 | - | • | - | - | - | |
| Veh in Median Storage | ,# 0 | - | 0 | - | - | 0 | |
| Grade, % | 0 | - | 0 | - | - | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| MVMT Flow | 58 | 3 | 296 | 99 | 5 | 1/4 | |
| | | | | | | | |
| Major/Minor N | Ainor1 | ١ | Aajor1 | 1 | Major2 | | |
| Conflicting Flow All | 530 | 346 | 0 | 0 | 395 | 0 | |
| Stage 1 | 346 | - | - | - | - | - | |
| Stage 2 | 184 | | - | - | - | - | |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - | |
| Critical Hdwy Stg 1 | 5.42 | | | - | - | - | |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - | |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - | |
| Pot Cap-1 Maneuver | 510 | 697 | • | - | 1164 | - | |
| Stage 1 | /16 | - | - | - | - | - | |
| Stage 2 | 848 | - | • | - | • | - | |
| Platoon blocked, % | 507 | 007 | • | - | 4404 | - | |
| Nov Cap-1 Maneuver | 507 | 097 | | - | 1104 | - | |
| Stage 1 | 712 | Celstalige | estreit | - | Constant | | |
| Stage 2 | 848 | - | | - | | _ | |
| Oldge 2 | 040 | | | | | | |
| | 14.00 | | | | | | |
| Approach | VVB | | NB | | SB | | |
| HCM Control Delay, s | 12.9 | | 0 | | 0.2 | | |
| ICM LOS | В | | | ter ser en ser se | | | |
| | | | | | | | |
| Minor Lane/Major Mvmi | t | NBT | NBRV | VBLn1 | SBL | SBT | |
| Capacity (veh/h) | | - | - | 515 | 1164 | - | |
| HCM Lane V/C Ratio | | - | - | 0.118 | 0.005 | - | |
| HCM Control Delay (s) | | - | - | 12.9 | 8.1 | 0 | |
| HCM Lane LOS | | - | - | В | Α | Α | |
| ICM 95th %tile Q(veh) | | - | - | 0.4 | 0 | - | |

Traffic Impact Analysis: Proposed Weston Trails Residential Development in Weston, Texas Page 48 of 59 October 12, 2020

| 13: FM 543 & S | treet | 5 | | | | | PM 2025 Site + Non-Site |
|------------------------|----------|--------------|------------|-------|-------------------|--|--|
| | | | | | | | |
| ntersection | | | | | | | |
| Int Delay, s/veh | 1 | | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | |
| Lane Configurations | W | | ħ | | | aî. | |
| Traffic Vol. veh/h | 35 | 2 | 214 | 61 | 3 | 130 | |
| Future Vol. veh/h | 35 | 2 | 214 | 61 | 3 | 130 | na este en la constante de |
| Conflicting Peds. #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | | None | - | None | 100 | None | |
| Storage Length | 0 | - | | - | - | - | |
| Veh in Median Storage | ,# 0 | - | 0 | - | - | 0 | |
| Grade, % | 0 | - | 0 | - | - | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles. % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Mymt Flow | 38 | 2 | 233 | 66 | 3 | 141 | |
| | | | | | - standprotection | and a state of the | |
| Major/Minor | Minor1 | N | Aaior1 | 1 | Maior2 | | |
| Conflicting Flow All | 413 | 266 | 0 | 0 | 299 | 0 | |
| Stage 1 | 266 | | | | | | |
| Stage 2 | 147 | - | • | | - | - | |
| Critical Hdwy | 6.42 | 6.22 | | | 4 12 | | |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 5.42 | | | _ | | 10000 | |
| Follow-up Hdwy | 3 518 | 3 318 | - | - | 2 218 | - | |
| Pot Cap-1 Maneuver | 595 | 773 | | | 1262 | | |
| Stage 1 | 779 | | - | - | - | - | |
| Stage 2 | 880 | - | | - | | | |
| Platoon blocked % | 000 | | - | - | | - | |
| Mov Cap-1 Maneuver | 593 | 773 | | _ | 1262 | _ | |
| Mov Cap-2 Maneuver | 593 | | - | - | 1202 | - | |
| Stage 1 | 777 | | | | | | |
| Stage 2 | 880 | | - | | | | |
| Jugo L | 000 | | | | | | |
| Approach | WB | | NB | | SB | | |
| HCM Control Delay | 11.4 | | 0 | | 0.2 | | |
| HCM LOS | В | | | | 0.02 | | |
| | | | | | | | |
| Minor Lane/Major Mvm | ıt | NBT | NBRV | VBLn1 | SBL | SBT | |
| Capacity (veh/h) | | - | - | 601 | 1262 | | |
| HCM Lane V/C Ratio | | - | - | 0.067 | 0.003 | - | |
| HCM Control Delay (s) | | - | - | 11.4 | 7.9 | 0 | |
| HCM Lane LOS | | - | - | B | A | A | |
| HCM 95th %tile Q(veh) | | | | 0.2 | 0 | | |
| Non our fund of Von | ALC: NO. | 171133555555 | Res Carlos | 0.2 | 0 | | |

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| 1.8 | | | | | | |
|--|--|--|--|--|---|---|
| 1.8 | | | | | | |
| The second s | | | | | | |
| WBL | WBR | NBT | NBR | SBL | SBT | |
| W | TILLI | î | TIDIT | 000 | A | |
| 53 | 3 | 125 | 91 | 5 | 80 | |
| 53 | 3 | 125 | 91 | 5 | 80 | |
| 0 | 0 | 0 | 0 | 0 | 0 | |
| Stop | Stop | Free | Free | Free | Free | |
| - | None | - | None | - | None | |
| 0 | - | - | - | - | - | |
| ,# 0 | • | 0 | - | - | 0 | |
| 0 | - 00 | 0 | - | - | 0 | |
| 92 | 92 | 92 | 92 | 92 | 92 | |
| 58 | 2 | 136 | 2 | 2 | 2 97 | |
| 50 | 5 | 150 | 33 | 0 | 01 | |
| linort | | laior1 | | Acior? | | |
| 283 | 196 | Algori | 0 | //ajorz | 0 | |
| 186 | 100 | - | 0 | 255 | 0 | |
| 97 | Contractor | | Contraction of the | - | - | |
| 6.42 | 6,22 | | | 4.12 | - | |
| 5.42 | - | | | - | - | |
| 5.42 | - | - | - | - | - | |
| 3.518 | 3.318 | - | - | 2.218 | - | |
| 707 | 856 | - | - | 1332 | - | |
| 846 | - | - | | - | - | |
| 927 | - | - | - | - | - | |
| 76.4 | | - | • | | - | |
| 704 | 856 | - | - | 1332 | - | |
| 704 | - | - | • | - | • | |
| 027 | - | - | - | - | - | |
| 921 | - | | - | - | - | |
| | and a second | NID | | 00 | | |
| M/P | | ALL A | | | | |
| WB 10.5 | | NB | | 0.5 | | |
| WB 10.5 | | 0 | | 0.5 | | |
| WB 10.5 B | | 0 | | 0.5 | | |
| WB 10.5 B | NBT | 0 NBRW | /BLn1 | 0.5 | SBT | |
| WB 10.5 B | NBT | NB 0 NBRW | /BLn1 711 | 0.5 SBL 1332 | SBT | |
| WB 10.5 B | NBT | NB 0 NBRV | VBLn1 711 0.086 | 0.5 SBL 1332 0.004 | SBT - | |
| WB 10.5 B | NBT - - | NBRV - - | VBLn1 711 0.086 10.5 | 0.5 SBL 1332 0.004 7.7 | SBT - - 0 | |
| WB 10.5 B | NBT - - - | <u>NBRV</u> - - - | VBLn1 711 0.086 10.5 B | 3B 0.5 SBL 1332 0.004 7.7 A | SBT - - 0 A | |
| | Vinor1 283 186 97 6.42 5.42 5.42 3.518 707 846 927 704 704 843 927 | U U Stop Stop - None 0 - 92 92 2 2 58 3 Vinor1 N 283 186 186 - 97 - 6.42 6.22 5.42 - 3.518 3.318 707 856 846 - 927 - 704 856 704 - 843 - 927 - | 0 0 0 Stop Stop Free - None - 0 - - 0 - 0 92 92 92 2 2 2 58 3 136 Vinor1 Major1 283 186 0 186 - - 97 - - 6.42 6.22 - 5.42 - - 5.42 - - 3.518 3.318 - 707 856 - 927 - - 704 856 - 704 - - 843 - - 927 - - | U U U U Stop Stop Free Free None - None 0 - 0 - 0 - 0 - 92 92 92 92 2 2 2 2 58 3 136 99 Vinor1 Major1 M 283 186 0 0 186 - - - 97 - - - 97 - - - 97 - - - 97 - - - 97 - - - 5.42 - - - 5.42 - - - 707 856 - - 927 - - - 704 856 - - 704 | O O O O O Stop Stop Free Free Free Free None - None - 0 - 0 - - 0 - 0 - - 90 - 0 - - 92 92 92 92 92 2 2 2 2 2 2 58 3 136 99 5 Winor1 Major1 Major2 283 186 0 0 235 186 - - - - 97 - - - - 97 - - - - 97 - - - - - 5.42 - - - - - 5.42 - - - - - | O None No No <thn< td=""></thn<> |

Appendix C3

2025 Mitigated AM & PM Traffic Conditions

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| 1: FM 543 & CF | R 206 | | | _ | | | AM 2025 Site + Non-Site with mitigation |
|------------------------|------------|-------|----------|--------|--------|------|---|
| Intersection | | | | | | | |
| Int Delay, s/veh | 8.6 | | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | |
| Lane Configurations | W | | 4 | 1 | | A | |
| Traffic Vol, veh/h | 301 | 21 | 103 | 105 | 18 | 299 | |
| Future Vol, veh/h | 301 | 21 | 103 | 105 | 18 | 299 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | 0 | - | - | 0 | - | - | |
| Veh in Median Storage | e, # 0 | - | 0 | - | - | 0 | |
| Grade, % | 0 | - | 0 | - | - | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Mvmt Flow | 327 | 23 | 112 | 114 | 20 | 325 | |
| | | | | | | | |
| Major/Minor | Minor1 | 1 | Aaior1 | | Major2 | | |
| Conflicting Flow All | 477 | 112 | 0 | 0 | 226 | 0 | |
| Stage 1 | 112 | - | - | - | - | - | |
| Stage 2 | 365 | - | - | | - | - | |
| Critical Hdwy | 6.42 | 6.22 | - | | 4 12 | | |
| Critical Hdwy Sto 1 | 5 42 | | - | - | | - | |
| Critical Hdwy Stg 2 | 5.42 | - | | | | | |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2,218 | - | |
| Pot Cap-1 Maneuver | 547 | 941 | | | 1342 | | |
| Stage 1 | 913 | - | - | - | - | - | |
| Stage 2 | 702 | - | | | | | |
| Platoon blocked. % | | | - | - | | - | |
| Mov Cap-1 Maneuver | 537 | 941 | | | 1342 | | |
| Nov Cap-2 Maneuver | 537 | - | - | | | - | |
| Stage 1 | 897 | | - | | - | - | |
| Stage 2 | 702 | - | - | - | - | - | |
| | | | | | | | |
| Approach | WB | | NB | | SB | | |
| HCM Control Delay | 22.1 | | 0 | | 0.4 | | |
| ICM LOS | C | | U | | 0.4 | | |
| | Ĩ | | | | | | |
| Minor Lane/Major Myr | nt | NBT | NBRV | VBI n1 | SBI | SBT | |
| Capacity (veh/h) | n. | - | - TADICY | 552 | 1342 | - | |
| CM Lane V/C Ratio | | - | | 0 634 | 0.015 | - | |
| -ICM Control Delay (s) | | | | 22.1 | 77 | 0 | |
| ICM Lena LOC | | | | C | Δ | Δ | |
| -Uvi ane Lus | | | - | 0 | A | 7 | |
| HCM 95th %tile O(veh) | CALCER ST. | | | 41 | | | |

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| 1: FM 543 & CF | R 206 | _ | | | | | PM 2025 Site + Non-Site with Mitigation |
|------------------------|--------|-------|--------|-------|--------|------|---|
| ntoronation | | | | | | | |
| nt Delay, s/veh | 4.9 | | | | | | |
| Vovement | WBL | WBR | NBT | NBR | SBL | SBT | |
| ane Configurations | W | | 4 | 1 | | ÷. | |
| Traffic Vol, veh/h | 205 | 26 | 337 | 344 | 27 | 186 | |
| Future Vol, veh/h | 205 | 26 | 337 | 344 | 27 | 186 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | | None | - | None | - | None | |
| Storage Length | 0 | - | - | 0 | - | - | |
| Veh in Median Storage | e,# 0 | - | 0 | - | - | 0 | |
| Grade, % | 0 | - | 0 | - | - | 0 | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Mvmt Flow | 223 | 28 | 366 | 374 | 29 | 202 | |
| | | | | | | | |
| Major/Minor | Minor1 | N | Aajor1 | | Major2 | | |
| Conflicting Flow All | 626 | 366 | 0 | 0 | 740 | 0 | 2 |
| Stage 1 | 366 | - | - | - | - | - | |
| Stage 2 | 260 | - | - | - | - | - | |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - | |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - | |
| Follow-up Hdwy | 3.518 | 3.318 | | - | 2.218 | | |
| Pot Cap-1 Maneuver | 448 | 679 | - | - | 867 | - | |
| Stage 1 | 702 | - | - | - | - | - | |
| Stage 2 | 783 | - | - | - | - | - | |
| Platoon blocked, % | | | - | - | | - | |
| Mov Cap-1 Maneuver | 431 | 679 | - | - | 867 | - | |
| Mov Cap-2 Maneuver | 431 | - | - | - | - | | |
| Stage 1 | 675 | - | - | - | - | - | |
| Stage 2 | 783 | - | - | - | - | - | |
| | | | | | | | |
| Approach | WB | | NB | | SB | | |
| HCM LOS | 22.1 | | 0 | | 1.2 | | |
| | U | | | | | | |
| Minor Lane/Major Mym | nt | NBT | NBRV | /BLn1 | SBL | SBT | |
| Capacity (veh/h) | | - | - | 449 | 867 | - | |
| -ICM Lane V/C Ratio | | - | - | 0.559 | 0.034 | | |
| -ICM Control Delay (s) | | - | - | 22.7 | 9.3 | 0 | |
| HCM Lane LOS | | | - | C | A | A | |
| HCM 95th %tile Q(veh) |) | - | - | 3.4 | 0.1 | | |
| | | | | | | | |

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Appendix D

Relevant Excerpts from the TxDOT Roadway Design and Access Management Manuals

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NOTE: Online users can click here to see this illustration in PDF format. (Metric)

Left-Turn Deceleration Lanes. Left-turn lanes on two-lane highways at intersecting crossroads generally are not economically justified. For certain moderate or high volume two-lane highways with heavy left-turn movements, however, left-turn lanes may be justified in view of reduced road user accident costs. <u>Figure 3-11</u> provides recommendations for when left-turn lanes should be considered based on traffic volumes.

Example: Traffic northbound on a highway has 350 vph with 10 percent left turns included. The southbound traffic volume is 200 vph. The design speed on the highway is 60 mph [100 km/h]. Beginning at the opposing volume (southbound in this case) of 200 vph, using the 10 percent left turn column and 60 mph [100 km/h] design speed section, a value of 330 vph advancing volume

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Chapter 3 — New Location and Reconstruction (4R) Design Criteria Section 4 — Two-Lane Rural Highways

(northbound) is found in the table. Because the northbound volume of 350 vph exceeds the table value of 330 vph, a left turn lane should be considered at the intersection.

Lengths of left-turn deceleration lanes are provided in Table 3-13.

Where used, left-turn lanes should be delineated with striping and pavement markers or jiggle bars. Passing should be restricted in advance of the intersection, and horizontal alignment shifts of the approaching travel lanes should be gradual. Figure 3-6 shows typical geometry for a rural two-lane highway with left-turn bays at a crossroad intersection.





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Chapter 3 — New Location and Reconstruction (4R) Design Criteria

Section 4 — Two-Lane Rural Highways

| Opposing Volume (vph) | Advancing Volume (vph) | | | | | | |
|--------------------------|------------------------|-----------------|-----------------|-----------------|--|--|--|
| - | 5 % Left Turns | 10 % Left Turns | 20 % Left Turns | 30 % Left Turns | | | |
| 40 mph [60 km/h] D | esign Speed | | | | | | |
| 800 | 330 | 240 | 180 | 160 | | | |
| 600 | 410 | 305 | 225 | 200 | | | |
| 400 | 510 | 380 | 275 | 245 | | | |
| 200 | 640 | 470 | 350 | 305 | | | |
| 100 | 720 | 515 | 390 | 340 | | | |
| 50 mph [80 km/h] D | esign Speed | | | | | | |
| 800 | 280 | 210 | 165 | 135 | | | |
| 600 | 350 | 260 | 195 | 170 | | | |
| 400 | 430 | 320 | 240 | 210 | | | |
| 200 | 550 | 400 | 300 | 270 | | | |
| 100 | 615 | 445 | 335 | 295 | | | |
| 60 mph [100 km/h] I | Design Speed | | | | | | |
| 800 | 230 | 170 | 125 | 115 | | | |
| 600 | 290 | 210 | 160 | 140 | | | |
| 400 | 365 | 270 | 200 | 175 | | | |
| 200 | 450 | 330 | 250 | 215 | | | |
| 100 | 505 | 370 | 275 | 240 | | | |

Right-Turn Deceleration Lanes. Shoulders 10 ft [3.0 m] wide alongside the traffic lanes generally provide sufficient area for acceleration or deceleration of right-turning vehicles. Where the right turn lane is being constructed in addition to the through lanes and shoulders, the minimum right turn lane width is 10 ft [3.0 m] with a 2 ft [0.6 m] surfaced shoulder. Where speed change lanes are used, they should be provided symmetrically along both sides of the highway for both directions of traffic, thus presenting drivers with a balanced section.

A deceleration-acceleration lane on one side of a two-lane highway, such as at a "tee" intersection, results in the appearance of a three-lane highway and may result in driver confusion. In this regard, right-turn speed change lanes are generally inappropriate for "tee" intersection design except where a four lane (2 through, 1 median left turn, 1 right acceleration/deceleration) section is provided.

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Chapter 3 — New Location and Reconstruction (4R) Design Criteria Section 4 — Two-Lane Rural Highways

Section 2, Figure 3-4 shows the lengths for right-turn deceleration lanes.

The length of a right-turn deceleration lane is the same as that for a left-turn lane (see Table 3-13). Right turn lanes shorter than the lengths given in Table 3-13 may be acceptable on some low volume rural highways.

Right-Turn Acceleration Lanes. Right-turn acceleration lanes may be appropriate on some twolane rural highways – for example on high volume highways where significant truck percentages are encountered. See <u>Table 3-10</u> for acceleration distances and taper lengths.

Intersections

The provision of adequate sight distance is of utmost importance in the design of intersections along two-lane rural highways. At intersections, consideration should be given to avoid steep profile grades as well as areas with limited horizontal or vertical sight distance. An intersection should not be situated just beyond a short crest vertical curve or a sharp horizontal curve. Where necessary, backslopes should be flattened and horizontal and vertical curves lengthened to provide additional sight distance. For more information on intersection sight distance, see <u>"Intersection Sight Distance"</u> in Chapter 2.

Desirably, the roadways should cross at approximately right angles. Where crossroad skew is flatter than 60 degrees to the highway, the crossroad should be re-aligned to provide for a near perpendicular crossing. The higher the functional classification, the closer to right-angle the crossroad intersection should be.

<u>"Minimum Designs for Truck and Bus Turns</u>" in Chapter 7 provides information regarding the accommodation of various types of truck class vehicles in intersection design. Further information on intersection design may also be found in AASHTO's A Policy on Geometric Design of Highways and Streets.

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Chapter 2 - Access-Management Standards

Section 3 — Number, Location, and Spacing of Access Connections

where heavy left-turn movements take place, but also occur where left-turn movements enter or leave driveways serving adjacent land development. As with left-turn movements, right-turn movements pose problems at both driveways and street intersections. Right-turn movements increase conflicts, delays, and crashes, particularly where a speed differential of 10 mph or more exists between the speed of through traffic and the vehicles that are turning right.

Table 2-3 presents thresholds for auxiliary lanes. These thresholds represent examples of where left turn and right turn lanes should be considered. Refer to the TxDOT *Roadway Design Manual*, Chapter 3, for proper acceleration and deceleration lengths.

| | Angelenstien | Developmention | Angelengting Daugherting | | |
|--|--|--|--|---|--|
| | Acceleration | Deceleration | Acceleration | Deceleration | |
| Non-Traversable (Raised Median) | (2) | All | Right turn egress > 200 vph (4) | ◆ >45 mph where right turn volume is > 50 vph (3) ◆ ≤45 where right turn volume is > 60 vph (3) | |
| Traversable (Undi- vided Road) | (2) | (1) | Same as above | Same as Above | |
| Conditions for prindicated in Table High crash ex Heavier than i Large volume Highways wh Conditions for N(Dense or built Where queues Where suffici (4) The acceleration i The distance from should be equal to Additionally, if the the back of the 0(| oviding an exclusive > 2-3: perience normal peak flow mo of truck traffic ere sight distance is li OT requiring a right-t t-out corridor where s of stopped vehicles ent length of property tane should not interfi- tane should not interfi- tane hould not interfi- hour access connection the percentile guaranterfi- hour access connection the percentile guaranterfi- tane fi- hour access connection the percentile guaranterfi- tane fi- hour access connection the percentile guaranterfi- tane fi- tane fi- hour access connection the percentile guaranterfi- tane fi- tane fi- tane fi | right-turn lane when the vements on the main re- imited urn lane where right-tu- pace is limited would block the access width is not available cre with any downstrea eration lane taper to the listances found in Table tion is signalized, the d | e right-turn traffic volu badway inn volumes are more the it to the right turn lane for the appropriate desi inn access connection. e next unsignalized dow e 2-2. istance from the end of t | ne projections are less than an indicated in Table 2-3: gn nstream access connection he acceleration lane taper t found Table 2-2 | |
| (5) Continuous right- cles. ^a Access connec | turn lanes can provid tions within a continu mbined with crossing | e mobility benefits bot tous right turn lane sho g left in movements, a | h for through movemen uld meet the spacing rec continuous right-turn lar | ts and for the turning vehi- puirements found in Table 2 te can introduce additional | |

Table 2-3: Auxiliary Lane Thresholds

Chapter 2 — Access Management Standards

Section 3 — Number, Location, and Spacing of Access Connections

Table 2-2: Other State Highways Connection Spacing Criteria

| Other State Highways Minimum Connection Spacing (1)(2)(| | |
|---|---------------|--|
| Posted Speed (mph) | Distance (ft) | |
| ≤ 30 | 200 | |
| 35 | 250 | |
| 40 | 305 | |
| 45 | 360 | |
| ≥ 50 | 425 | |

(1) Distances are for passenger cars on level grade. These distances may be adjusted for downgrades and/or significant truck traffic. Where present or projected traffic operations indicate specific needs, consideration may be given to intersection sight distance and operational gap acceptance measurement adjustments.

(2) When these values are not attainable, refer to the variance process as described in Chapter 2, Section 5.

(3) Access spacing values shown in this table do not apply to rural highways outside of metropolitan planning organization boundaries where there is little, if any, potential for development with current ADT levels below 2000. Access connection spacing below the values shown in this table may be approved based on safety and operational considerations as determined by TxDOT.

Corner clearance refers to the separation of access connections from roadway intersections. Table 2-2 provides minimum corner clearance criteria.

Where adequate access connection spacing cannot be achieved, the permitting authority may allow for a lesser spacing when shared access is established with an abutting property. Where no other alternatives exist, construction of an access connection may be allowed along the property line farthest from the intersection. To provide reasonable access under these conditions but also provide the safest operation, consideration should be given to designing the driveway connection to allow only the right-in turning movement or only the right-in/right out turning movements if feasible.

Auxiliary Lanes

This subsection describes the basic use and functional criteria associated with auxiliary lanes. Auxiliary lanes consist of left-turn and right-turn movements, deceleration, acceleration, and their associated transitions and storage requirements. Left-turn movements may pose challenges at driveways and street intersections. They may increase conflicts, delays, and crashes and often complicate traffic signal timing. These problems are especially acute at major highway intersections

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